

# The POG Technique for Modeling Planetary Gears and Hybrid Automotive Systems



UNIVERSITÀ DEGLI STUDI  
DI MODENA E REGGIO EMILIA

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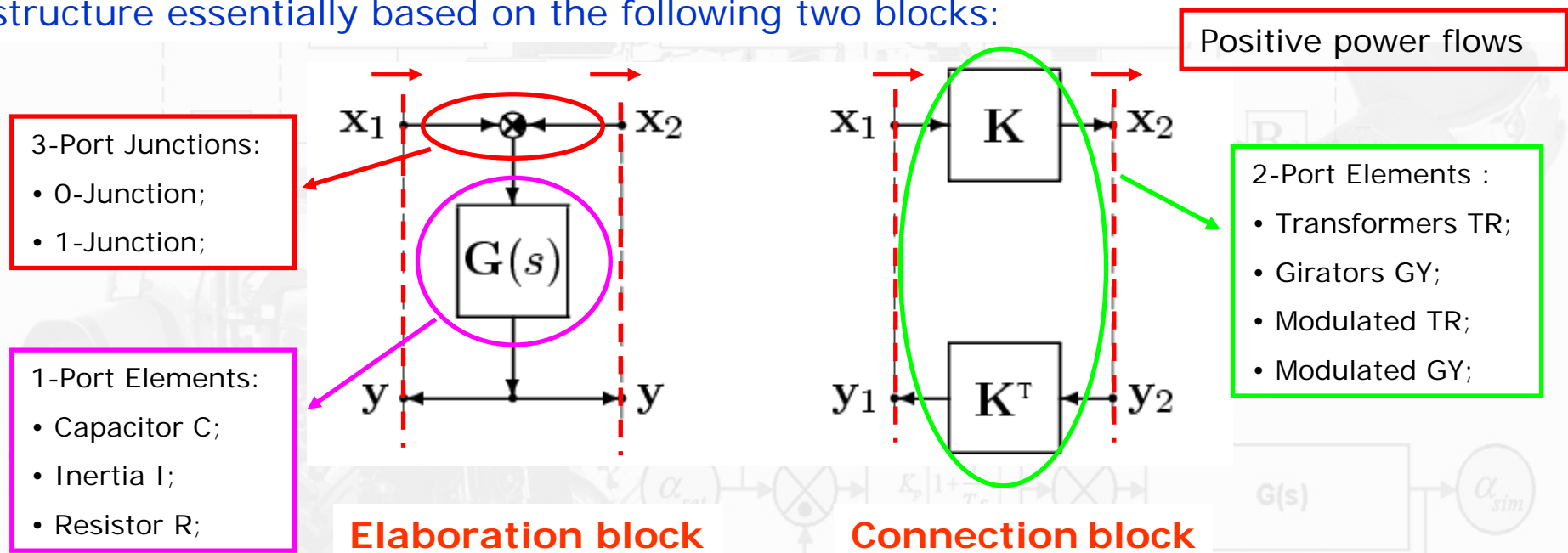
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## Outline

- 1) The Power-Oriented Graphs technique (intro)
- 2) POG modeling of a Planetary Gear
  - a) system transformation and system reduction
  - b) different dynamic models
- 3) POG modeling of an Hybrid Automotive System
- 4) Simulations and control
- 5) Conclusions

# Power-Oriented Graphs (POG)

The Power-Oriented Graphs are "block diagrams" obtained by using a "modular" structure essentially based on the following two blocks:



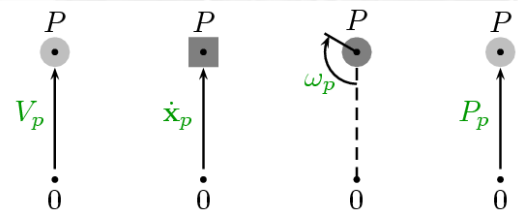
- POG maintains a direct correspondence between pairs of system variables and real power flows: the product of the two variables involved in each dashed line of the graph has the physical meaning of "power flowing through that section".
- The Elaboration block can store and dissipate/generate energy.
- The Connection block can only "transform" the energy.

# POG dynamic modeling: electrical example

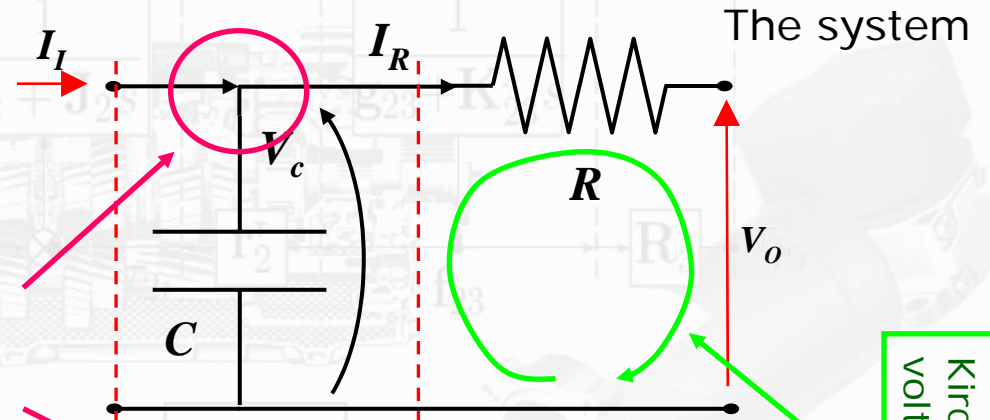
Across and through variables:

	POG Variables	
<b>Domains:</b>	Across: $v_e$	Through: $v_f$
Electrical	Voltage $V$	Current $I$
Mec. Tra.	Velocity $v$	Force $F$
Mec. Rot.	Ang. Vel. $\omega$	Torque $\tau$
Hydraulic	Pressure $P$	Flow rate $Q$

Across variables are defined between two points:

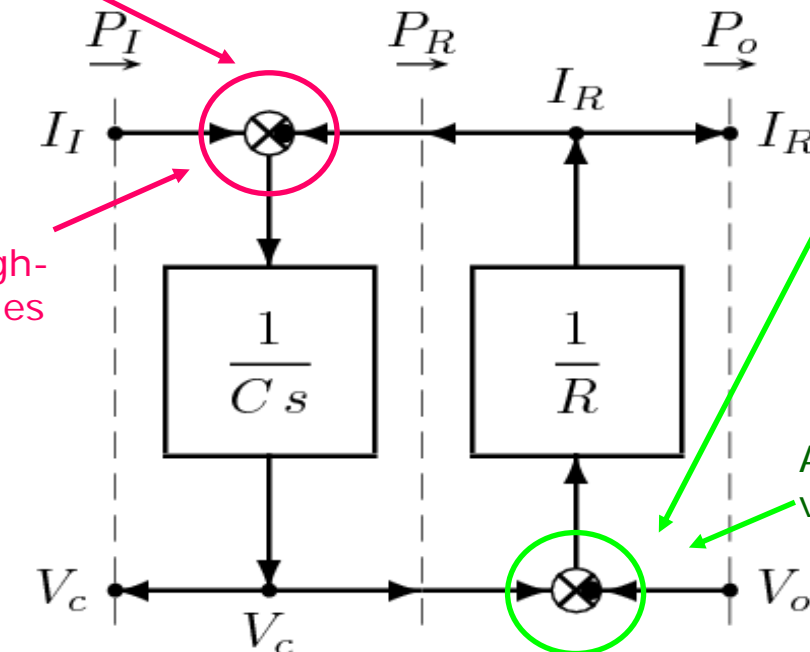


Through variables are defined in a single point:



Kirchhoff's current law

Kirchhoff's voltage law



Through-variables

Across-variables

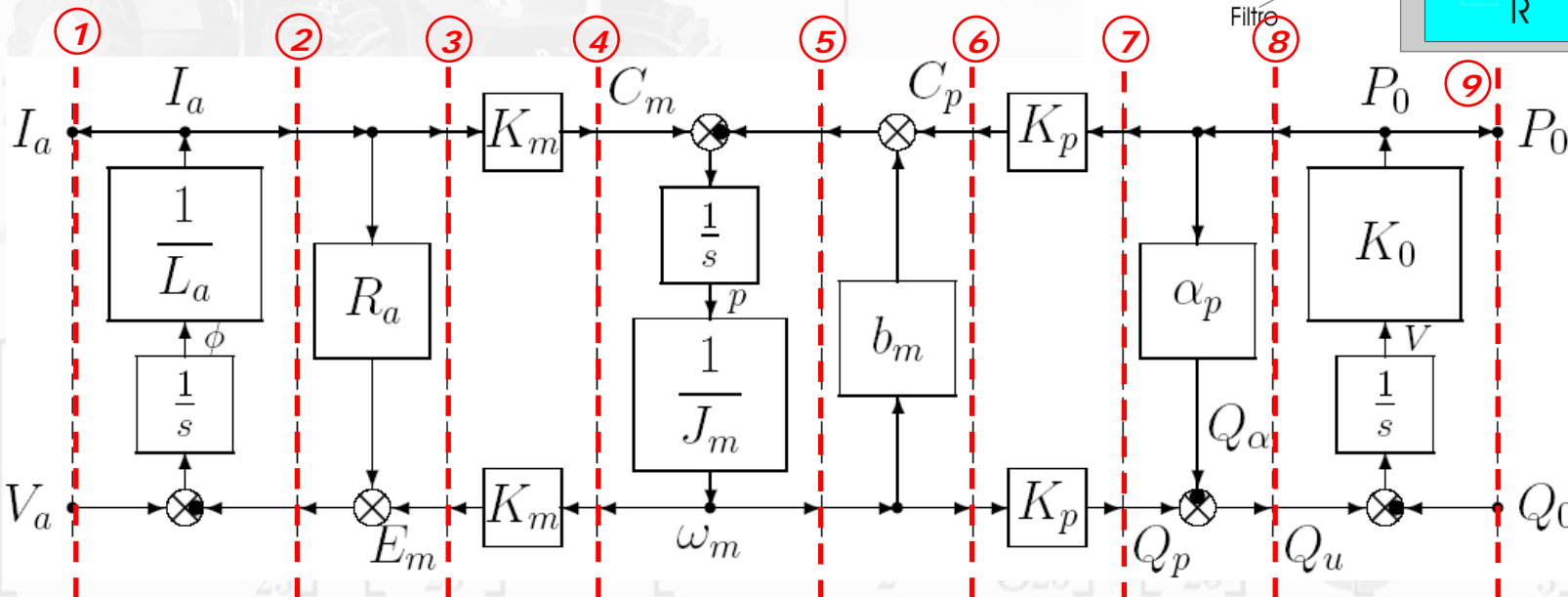
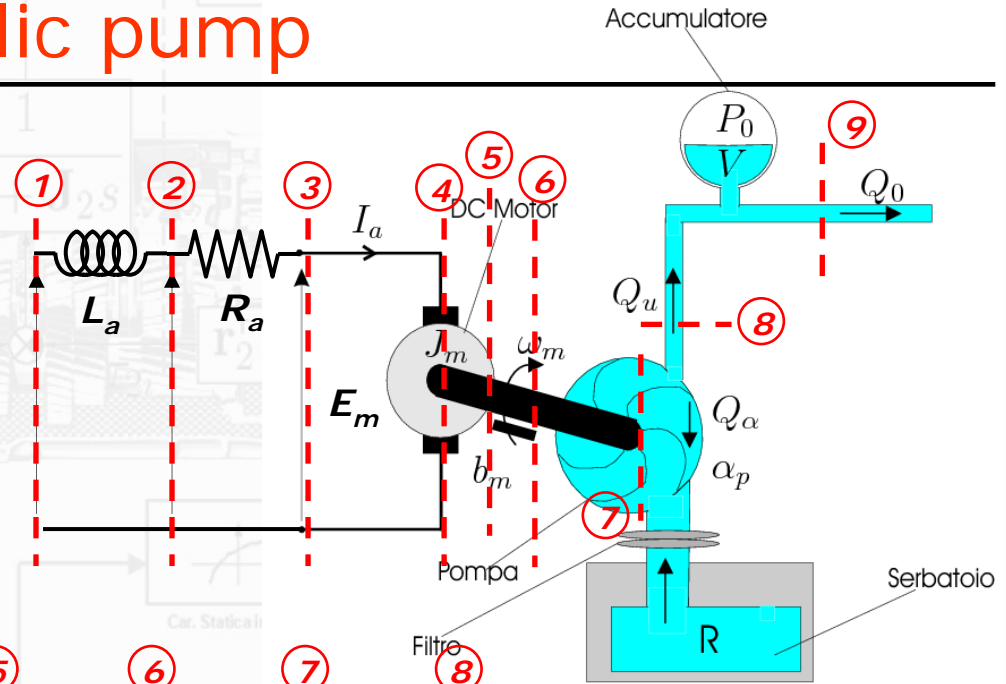
The POG model

# Example of POG modeling: DC electric motor with an hydraulic pump

A DC motor connected to an hydraulic pump:

There is a direct correspondence between the POG blocks and the physical elements ...

The POG model:

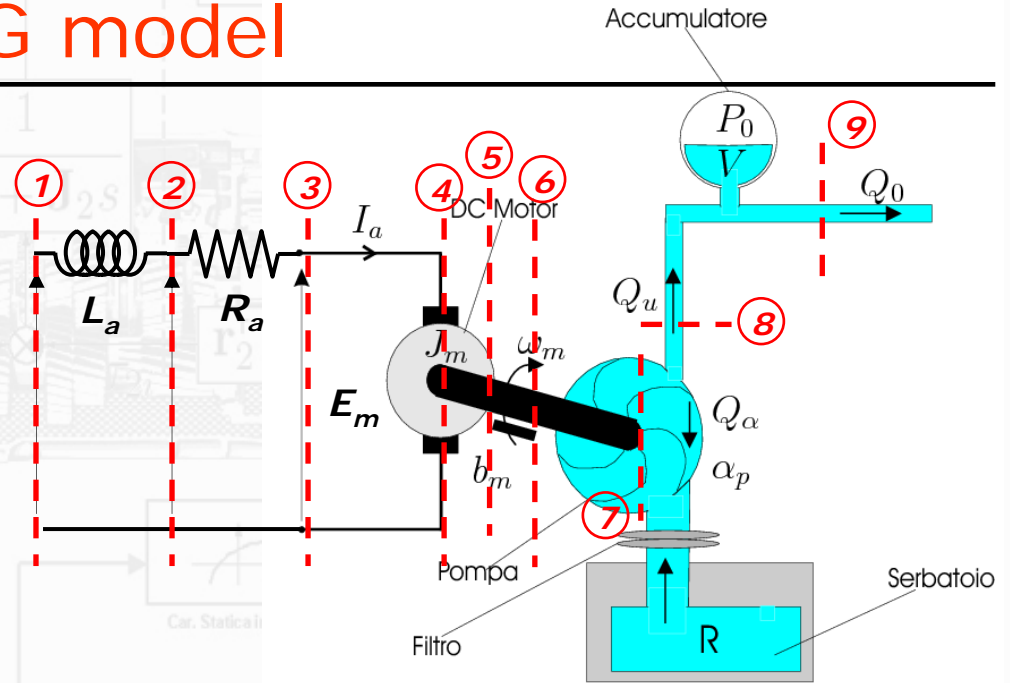


POG models can be directly inserted in Simulink.

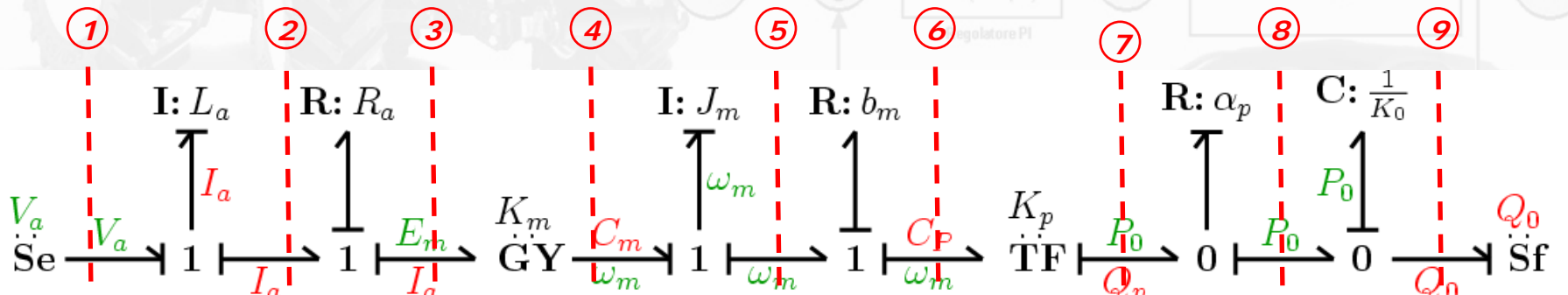
# DC electric motor with an hydraulic pump: comparison with the BG model

A DC motor connected to an hydraulic pump:

- + The graphical representation is more flexible and more compact.
- Not easy for the beginners.
- Not direct use in Simulink.



The Bond Graph model:



# Introduction

## Power-Oriented Graphs - LTI Systems

The POG state space description of the DC motor with hydraulic pump:

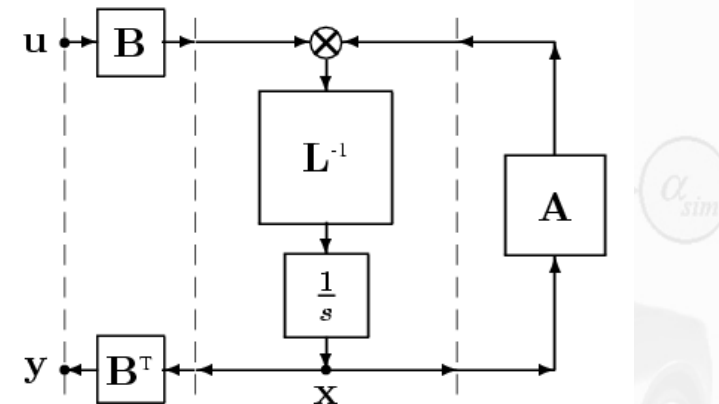
$$\underbrace{\begin{bmatrix} L_a & 0 & 0 \\ 0 & \cancel{J_m} & 0 \\ 0 & 0 & \frac{1}{K_0} \end{bmatrix}}_{\mathbf{L}} \underbrace{\begin{bmatrix} \dot{I}_a \\ \dot{\omega}_m \\ \dot{P}_0 \end{bmatrix}}_{\dot{\mathbf{x}}} = \underbrace{\begin{bmatrix} -R_a & -K_m & 0 \\ K_m & -b_m & -K_p \\ 0 & K_p & -\alpha_p \end{bmatrix}}_{\mathbf{A}} \underbrace{\begin{bmatrix} I_a \\ \omega_m \\ P_0 \end{bmatrix}}_{\mathbf{x}} + \underbrace{\begin{bmatrix} 1 & 0 \\ 0 & 0 \\ 0 & -1 \end{bmatrix}}_{\mathbf{B}} \underbrace{\begin{bmatrix} V_a \\ Q_0 \end{bmatrix}}_{\mathbf{u}} \quad \mathbf{y} = \underbrace{\begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}}_{\mathbf{C}} \mathbf{x}$$

- Direct correspondence between POG and state space descriptions:

$$\left\{ \begin{array}{l} \mathbf{L}\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u} \\ \mathbf{y} = \mathbf{B}^T\mathbf{x} \end{array} \right. \quad \begin{array}{l} \text{Energy matrix} \\ \text{Power matrix} \end{array}$$

Stored Energy:  $E_s = \frac{1}{2} \mathbf{x}^T \mathbf{L} \mathbf{x}$

Dissipating Power:  $P_d = \mathbf{x}^T \mathbf{A} \mathbf{x}$



- With POG it is easy to obtain reduced models of the system

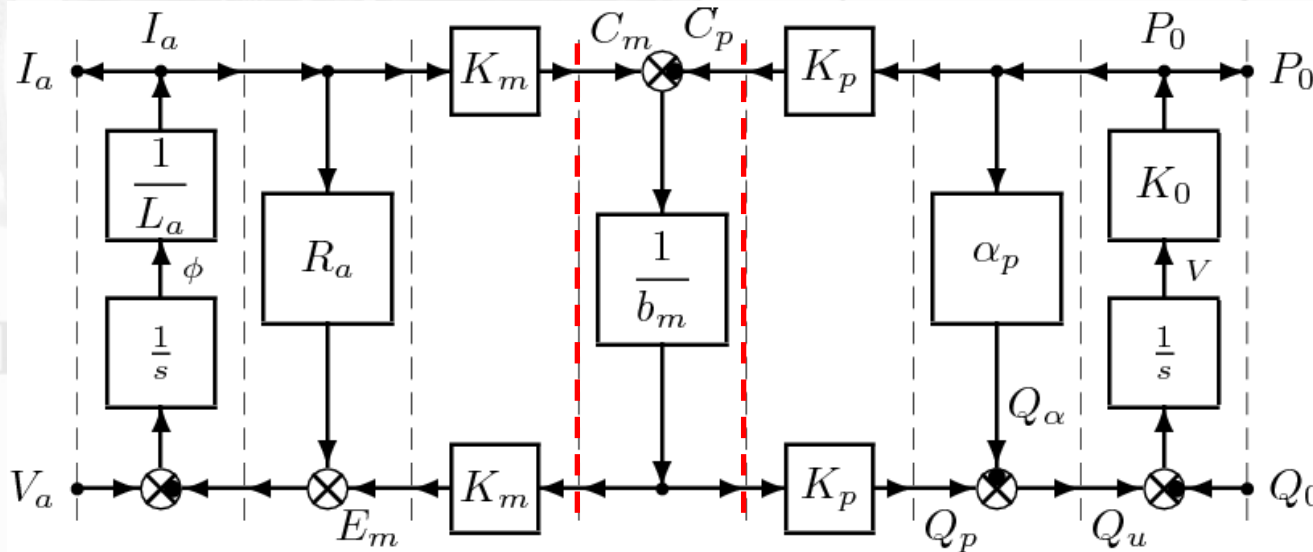
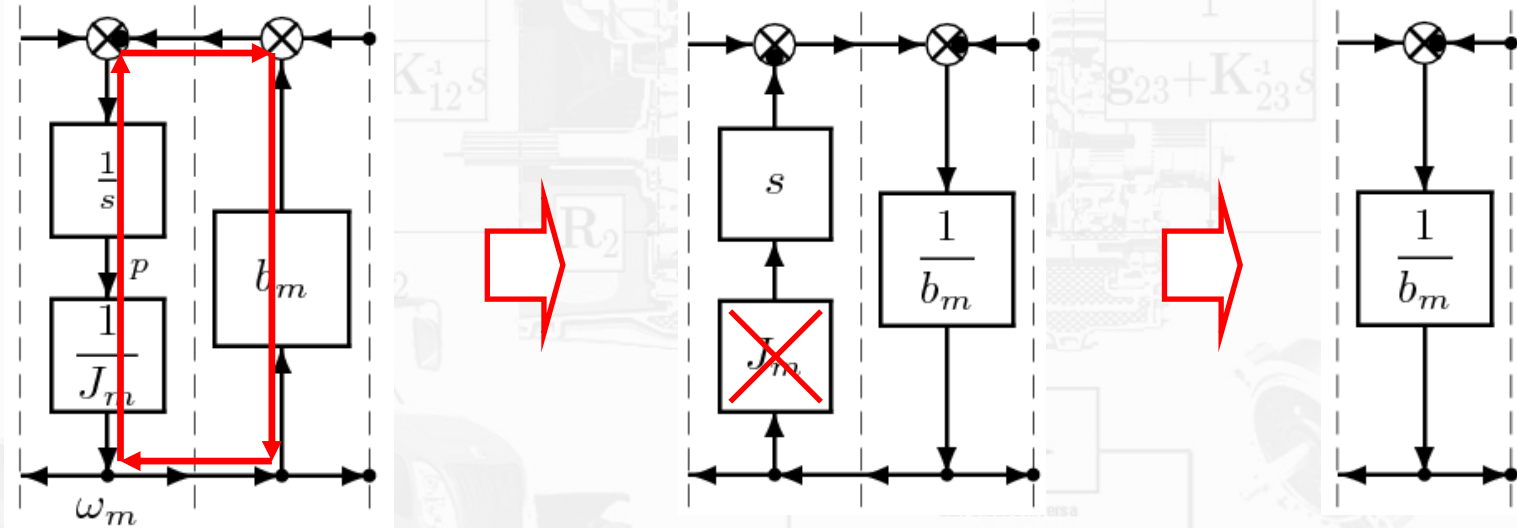
Which is the "reduced model" when  $J_m \rightarrow 0$ ?



Two possible solutions:

- graphically inverting a path ...;
- using a congruent transformation

# POG modeling reduction: graphically inverting a path



POG reduced model !

# POG modeling reduction: using a “congruent” transformation

When an eigenvalue of matrix  $L$  goes to zero (or to infinity), the system degenerates towards a lower dynamic dimension system. The “reduced system” can be obtained by using a congruent transformation  $x=Tz$  where  $T$  is a rectangular matrix:

$$\left\{ \begin{array}{l} \mathbf{T}^T \mathbf{L} \mathbf{T} \dot{\mathbf{z}} = \mathbf{T}^T \mathbf{A} \mathbf{T} \mathbf{z} + \mathbf{T}^T \mathbf{B} \mathbf{u} \\ \mathbf{y} = \mathbf{B}^T \mathbf{T} \mathbf{z} \end{array} \right. \Leftrightarrow \left\{ \begin{array}{l} \bar{\mathbf{L}} \dot{\mathbf{z}} = \bar{\mathbf{A}} \mathbf{z} + \bar{\mathbf{B}} \mathbf{u} \\ \mathbf{y} = \bar{\mathbf{B}}^T \mathbf{z} \end{array} \right.$$

congruent transformation Transformed system

When a parameter goes to zero a static relation between state variable arises:

$$J_m = 0 \quad \Rightarrow \quad K_m I_a - b_m \omega_m - K_p P_0 = 0 \quad \Rightarrow \quad \omega_m = \frac{K_m}{b_m} I_a - \frac{K_p}{b_m} P_0$$

A rectangular state space transformation can be easily obtained:

$$\underbrace{\begin{bmatrix} I_a \\ \omega_m \\ P_0 \end{bmatrix}}_{\mathbf{x}} = \underbrace{\begin{bmatrix} 1 & 0 \\ \frac{K_m}{b_m} & -\frac{K_p}{b_m} \\ 0 & 1 \end{bmatrix}}_{\mathbf{T}} \underbrace{\begin{bmatrix} I_a \\ P_0 \end{bmatrix}}_{\mathbf{z}}$$

Old state vector Rectangular matrix New state vector

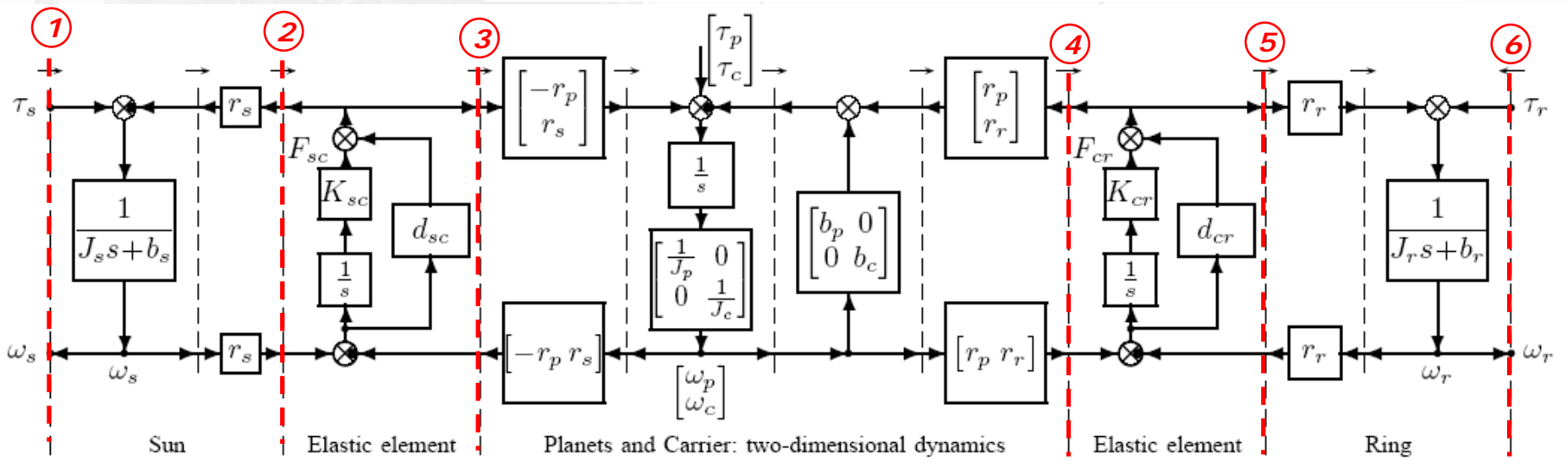
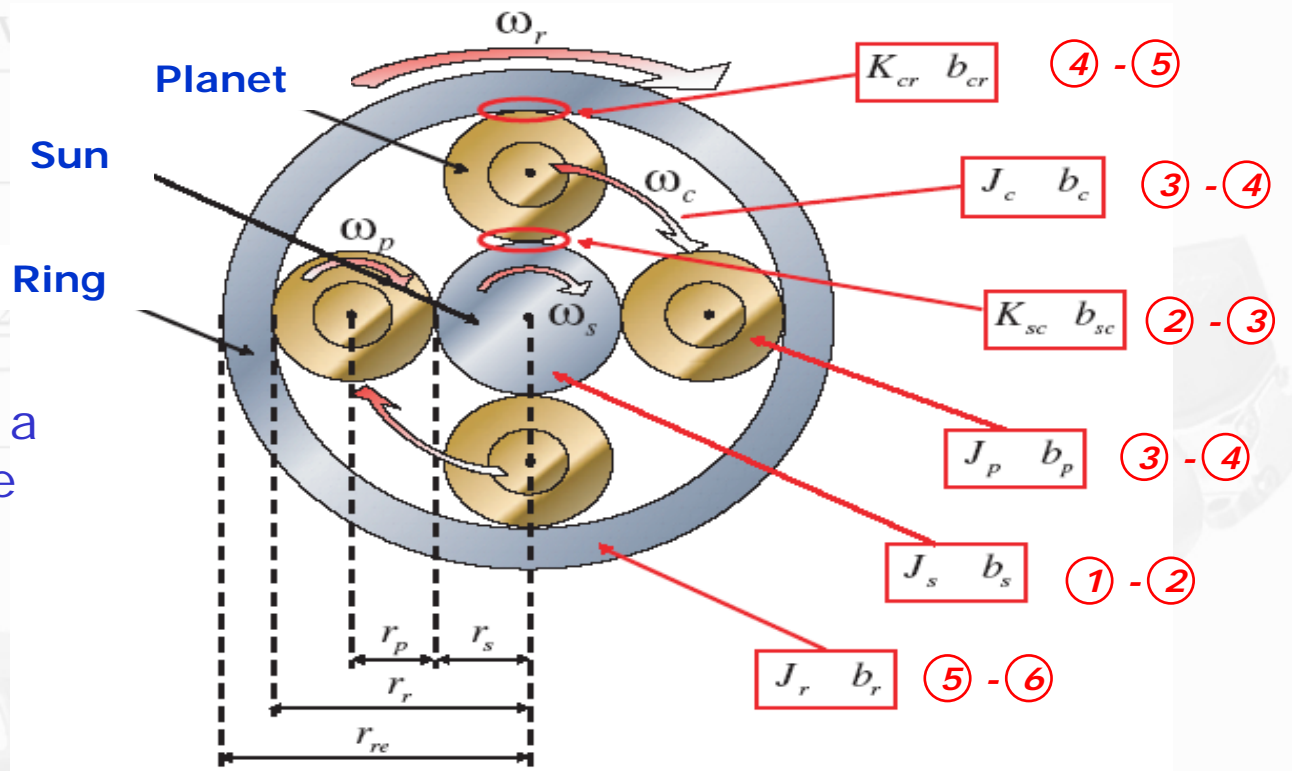
Applying the congruent transformation one directly obtains the reduced system:

$$\begin{bmatrix} L_a & 0 \\ 0 & \frac{1}{K_0} \end{bmatrix} \begin{bmatrix} \dot{I}_a \\ \dot{P}_0 \end{bmatrix} = \begin{bmatrix} -R_a - \frac{K_m^2}{b_m} & \frac{K_m K_p}{b_m} \\ \frac{K_m K_p}{b_m} & -\alpha_p - \frac{K_p^2}{b_m} \end{bmatrix} \begin{bmatrix} I_a \\ P_0 \end{bmatrix} + \begin{bmatrix} 1 & 0 \\ 0 & -1 \end{bmatrix} \begin{bmatrix} V_a \\ Q_0 \end{bmatrix}$$

# Modeling a Planetary Gear

The POG blocks have a direct correspondence with the physical elements.

The POG model:



# Planetary Gear: state space model

From the POG block scheme directly follows the dynamic state space model of the system (n=6):

$$\bar{\mathbf{L}} \dot{\bar{\mathbf{x}}} = -\bar{\mathbf{A}} \bar{\mathbf{x}} + \bar{\mathbf{B}} \mathbf{u},$$

$$\mathbf{y} = \bar{\mathbf{B}}^T \bar{\mathbf{x}}$$

State vector:

$$\bar{\mathbf{x}} = \begin{bmatrix} \omega_s \\ F_{sc} \\ \omega_p \\ \omega_c \\ F_{cr} \\ \omega_r \end{bmatrix}$$

Energy matrix:

$$\bar{\mathbf{L}} = \begin{bmatrix} J_s & 0 & 0 & 0 & 0 & 0 \\ 0 & \frac{1}{K_{sc}} & 0 & 0 & 0 & 0 \\ 0 & 0 & J_p & 0 & 0 & 0 \\ 0 & 0 & 0 & J_c & 0 & 0 \\ 0 & 0 & 0 & 0 & \frac{1}{K_{cr}} & 0 \\ 0 & 0 & 0 & 0 & 0 & J_r \end{bmatrix}$$

Input matrix:

$$\bar{\mathbf{B}} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Power matrix:

$$\bar{\mathbf{A}} = - \begin{bmatrix} -b_s - r_s^2 d_{sc} & -r_s & -r_s d_{sc} r_p & r_s^2 d_{sc} & 0 & 0 \\ r_s & 0 & r_p & -r_s & 0 & 0 \\ -r_s d_{sc} r_p & -r_p & -b_p - d_{sc} r_p^2 - d_{cr} r_p^2 & r_s d_{sc} r_p - d_{cr} r_p r_r & -r_p & d_{cr} r_p r_r \\ r_s^2 d_{sc} & r_s & r_s d_{sc} r_p - d_{cr} r_p r_r & -b_c - r_s^2 d_{sc} - d_{cr} r_r^2 & -r_r & d_{cr} r_r^2 \\ 0 & 0 & r_p & r_r & 0 & -r_r \\ 0 & 0 & d_{cr} r_p r_r & d_{cr} r_r^2 & r_r & -b_r - d_{cr} r_r^2 \end{bmatrix}$$

Is this model too complex?



POG technique provides the reduced models when the stiffness tend to infinity or the inertias tend to zero.

# Planetary gear: reduced inertial model

When the stiffness coefficients tend to infinity  $K_{cr} \rightarrow \infty$ ,  $K_{sc} \rightarrow \infty$  a static relation between the state variables appears:

$$\mathbf{x}_2 = \begin{bmatrix} \omega_p \\ \omega_r \end{bmatrix} = -\mathbf{A}_{32}^{-1} \mathbf{A}_{31} \mathbf{x}_1 = \begin{bmatrix} -\frac{r_s}{r_p} & \frac{r_s}{r_p} \\ -\frac{r_s}{r_r} & 1 + \frac{r_s}{r_r} \end{bmatrix} \begin{bmatrix} \omega_s \\ \omega_c \end{bmatrix}$$

Applying a rectangular and congruent state space transformation  $\mathbf{x} = \mathbf{T}_2 \mathbf{x}_1$

where:

$$\mathbf{T}_2 = \begin{bmatrix} \mathbf{I}_2 \\ -\mathbf{A}_{32}^{-1} \mathbf{A}_{31} \\ 0 \end{bmatrix}$$

one obtains the transformed and reduced system:

$$\begin{aligned} \mathbf{L}_r \dot{\mathbf{x}}_1 &= -\mathbf{A}_r \mathbf{x}_1 + \mathbf{B}_r \mathbf{u} \\ \mathbf{y} &= \mathbf{B}_r^T \mathbf{x}_1 \end{aligned}$$

Matrices  $\mathbf{L}_r = \mathbf{T}_2^T \mathbf{L} \mathbf{T}_2$ ,  $\mathbf{A}_r = \mathbf{T}_2^T \mathbf{A} \mathbf{T}_2$  and  $\mathbf{B}_r = \mathbf{T}_2^T \mathbf{B}$  have the following structure:

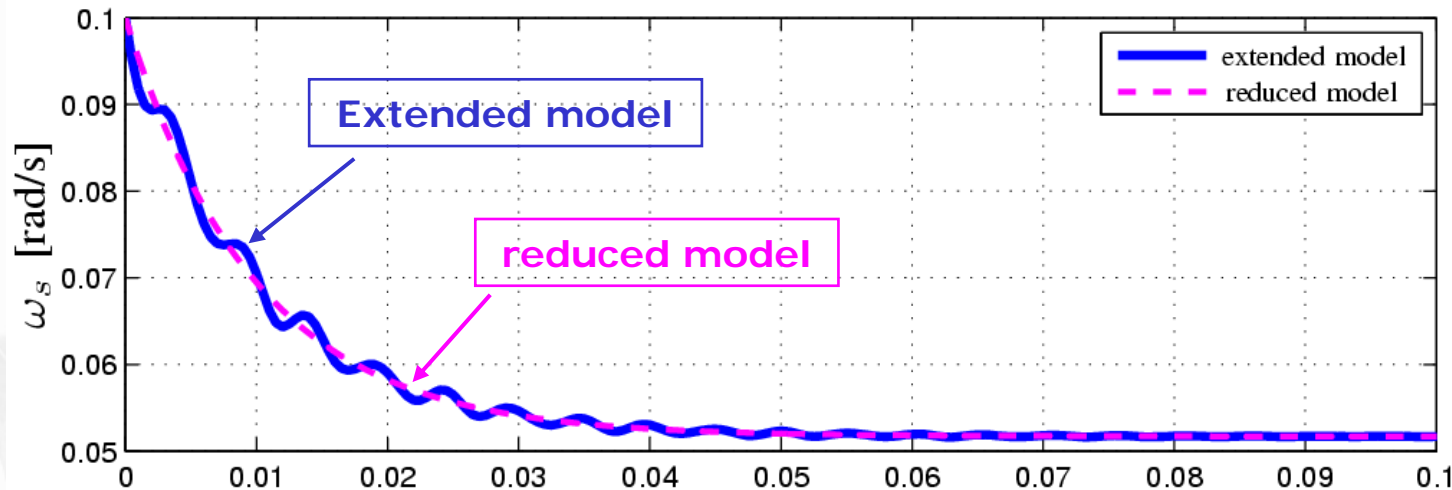
$$\mathbf{L}_r = \begin{bmatrix} J_s + \frac{r_s^2}{r_p^2} J_p + \frac{r_s^2}{r_r^2} J_r & -\frac{r_s^2}{r_p^2} J_p - \frac{r_s}{r_r} \left(1 + \frac{r_s}{r_r}\right) J_r \\ -\frac{r_s^2}{r_p^2} J_p - \frac{r_s}{r_r} \left(1 + \frac{r_s}{r_r}\right) J_r & J_c + \frac{r_s^2}{r_p^2} J_p + \left(1 + \frac{r_s}{r_r}\right)^2 J_r \end{bmatrix}$$

$$\mathbf{A}_r = \begin{bmatrix} b_s + \frac{r_s^2}{r_p^2} b_p + \frac{r_s^2}{r_r^2} b_r & -\frac{r_s^2}{r_p^2} b_p - \frac{r_s}{r_r} \left(1 + \frac{r_s}{r_r}\right) b_r \\ -\frac{r_s^2}{r_p^2} b_p - \frac{r_s}{r_r} \left(1 + \frac{r_s}{r_r}\right) b_r & b_c + \frac{r_s^2}{r_p^2} b_p + \left(1 + \frac{r_s}{r_r}\right)^2 b_r \end{bmatrix}$$

$$\mathbf{B}_r = \begin{bmatrix} 1 & 0 & -\frac{r_s}{r_r} \\ 0 & 1 & 1 + \frac{r_s}{r_r} \end{bmatrix} \quad \mathbf{x}_1 = \begin{bmatrix} \omega_s \\ \omega_c \end{bmatrix} \quad \mathbf{y} = \begin{bmatrix} \omega_s \\ \omega_c \\ \omega_r \end{bmatrix}$$

# Reduced inertial model: simulation results

Comparison between the extended and reduced models:



Parameters used in simulation (SI):  $[J_s, b_s, r_s] = [0.049, 4.946, 0.102]$   
 $[J_r, b_r, r_r] = [2.180, 218.02, 0.248]$   $[J_p, b_p, r_p] = [0.081, 8.123, 0.073]$   
 $[J_c, b_c] = [0.929, 92.89]$   $[K_{sc}, d_{sc}] = [K_{cr}, d_{cr}] = [10^7, 10]$   $[\tau_s, \tau_c, \tau_r] = [0, 4, 0]$   
 $[\omega_s(0), \omega_c(0), \omega_r(0)] = [0.1, -0.2, -0.323]$

Note: the use of a “rectangular” matrix for transforming and reducing a dynamical system is a “specific characteristics” of the POG technique.

# Planetary gear: reduced elastic model

When the inertias coefficients tend to zero  $J_s = J_c = J_r = 0$  a static relation between the state and input variables appears in the system:

$$\mathbf{z}_2 = -\mathbf{A}_{22}^{-1}\mathbf{A}_{21}\mathbf{z}_1 - \mathbf{A}_{22}^{-1}\mathbf{B}_2\mathbf{u} \quad \text{where} \quad \mathbf{z}_1 = \begin{bmatrix} F_{sc} \\ \omega_p \\ F_{cr} \end{bmatrix} \quad \mathbf{z}_2 = \begin{bmatrix} \omega_s \\ \omega_c \\ \omega_r \end{bmatrix} \quad \mathbf{B}_2 = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$\mathbf{A}_{22} = \begin{bmatrix} -b_s - r_s^2 d_{sc} & r_s^2 d_{sc} & 0 \\ r_s^2 d_{sc} & -b_c - r_s^2 d_{sc} - r_r^2 d_{cr} & r_r^2 d_{cr} \\ 0 & r_r^2 d_{cr} & -b_r - r_r^2 d_{cr} \end{bmatrix} \quad \mathbf{A}_{21} = \begin{bmatrix} -r_s & -r_s d_{sc} r_p & 0 \\ r_s & r_s d_{sc} r_p - r_p r_r d_{cr} & -r_r \\ 0 & r_p r_r d_{cr} & r_r \end{bmatrix}$$

Applying a congruent transformation and inverting the system one obtains the POG reduced elastic model:

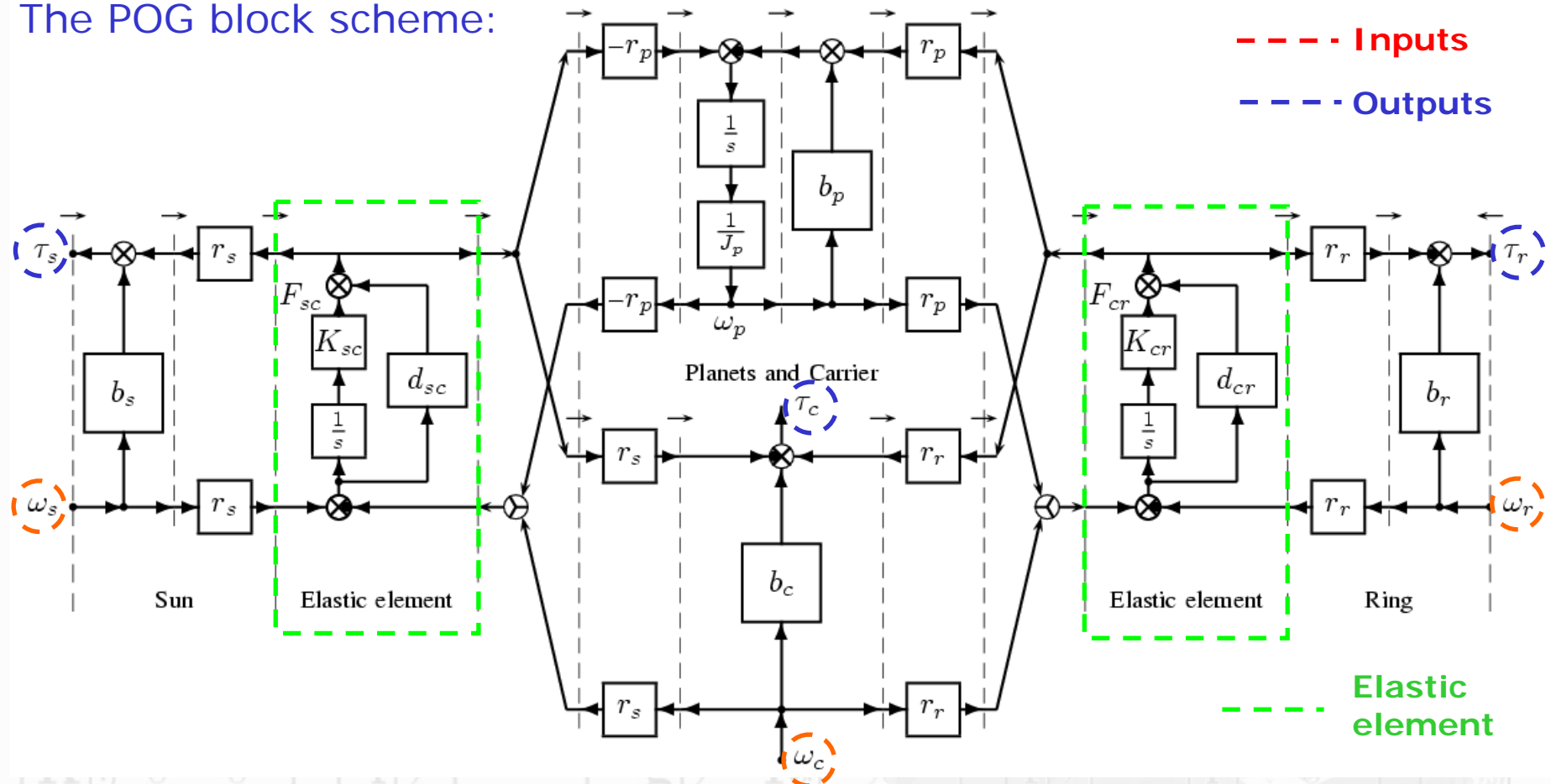
$$\mathbf{z} = \begin{bmatrix} \mathbf{I}_2 \\ -\mathbf{A}_{22}^{-1}\mathbf{A}_{21} \end{bmatrix} \mathbf{z}_1 + \begin{bmatrix} 0 \\ -\mathbf{A}_{22}^{-1}\mathbf{B}_2 \end{bmatrix} \mathbf{u}$$

$$\underbrace{\begin{bmatrix} \frac{1}{K_{sc}} & 0 & 0 \\ 0 & J_p & 0 \\ 0 & 0 & \frac{1}{K_{cr}} \end{bmatrix}}_{\tilde{\mathbf{L}}_e} \underbrace{\begin{bmatrix} \dot{F}_{sc} \\ \dot{\omega}_p \\ \dot{F}_{cr} \end{bmatrix}}_{\dot{\tilde{\mathbf{x}}}} = \underbrace{\begin{bmatrix} 0 & r_p & 0 \\ -r_p & -r_p^2 d_{sc} - b_p - r_p^2 d_{cr} & -r_p \\ 0 & r_p & 0 \end{bmatrix}}_{-\tilde{\mathbf{A}}_e} \underbrace{\begin{bmatrix} F_{sc} \\ \omega_p \\ F_{cr} \end{bmatrix}}_{\tilde{\mathbf{x}}} + \underbrace{\begin{bmatrix} r_s & -r_s & 0 \\ -r_s d_{sc} r_p & r_s d_{sc} r_p - r_r d_{cr} r_p & r_r d_{cr} r_p \\ 0 & r_r & -r_r \end{bmatrix}}_{\tilde{\mathbf{B}}_e} \underbrace{\begin{bmatrix} \omega_s \\ \omega_c \\ \omega_r \end{bmatrix}}_{\tilde{\mathbf{u}}} \quad \text{Inputs}$$

$$\underbrace{\begin{bmatrix} \tau_s \\ \tau_c \\ \tau_r \end{bmatrix}}_{\mathbf{y}} = \underbrace{\begin{bmatrix} r_s & r_s d_{sc} r_p & 0 \\ -r_s & -r_s d_{sc} r_p + r_r d_{cr} r_p & r_r \\ 0 & -r_r d_{cr} r_p & -r_r \end{bmatrix}}_{\tilde{\mathbf{C}}_e} \underbrace{\begin{bmatrix} F_{sc} \\ \omega_p \\ F_{cr} \end{bmatrix}}_{\tilde{\mathbf{x}}} + \underbrace{\begin{bmatrix} b_s + r_s^2 d_{sc} & -r_s^2 d_{sc} & 0 \\ -r_s^2 d_{sc} & b_c + r_s^2 d_{sc} + r_r^2 d_{cr} & -r_r^2 d_{cr} \\ 0 & -r_r^2 d_{cr} & b_r + r_r^2 d_{cr} \end{bmatrix}}_{\tilde{\mathbf{D}}_e} \underbrace{\begin{bmatrix} \omega_s \\ \omega_c \\ \omega_r \end{bmatrix}}_{\tilde{\mathbf{u}}}$$

# Reduced and inverted elastic model

The POG block scheme:



A dissipative reduced system is obtained when  $J_s = J_c = J_r = 0$  and  $K_{sc} = K_{cr} = \infty$ :

$$r_s \omega_s - (r_r + r_s) \omega_c + r_r \omega_r = 0$$

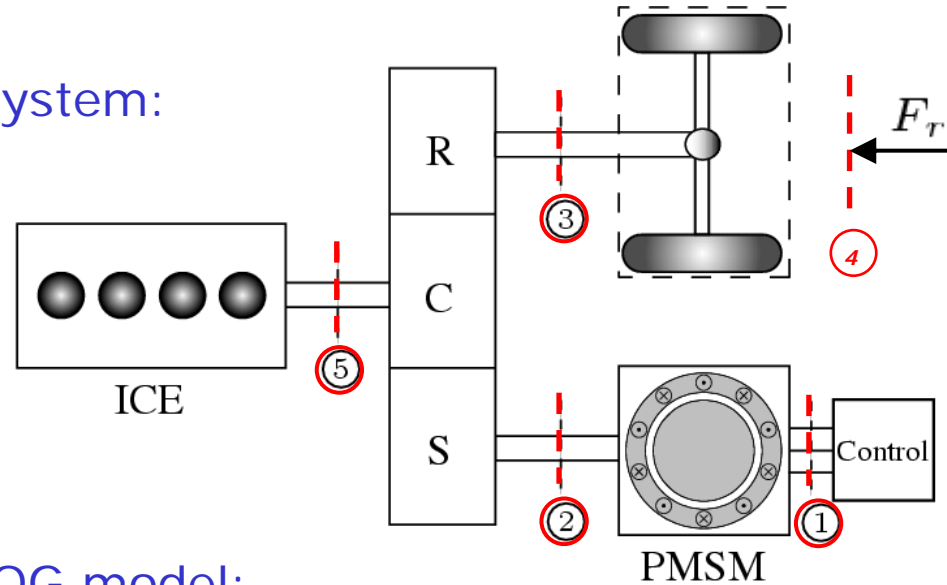
# POG model of Hybrid Automotive Systems

A parallel Hybrid Automotive System:

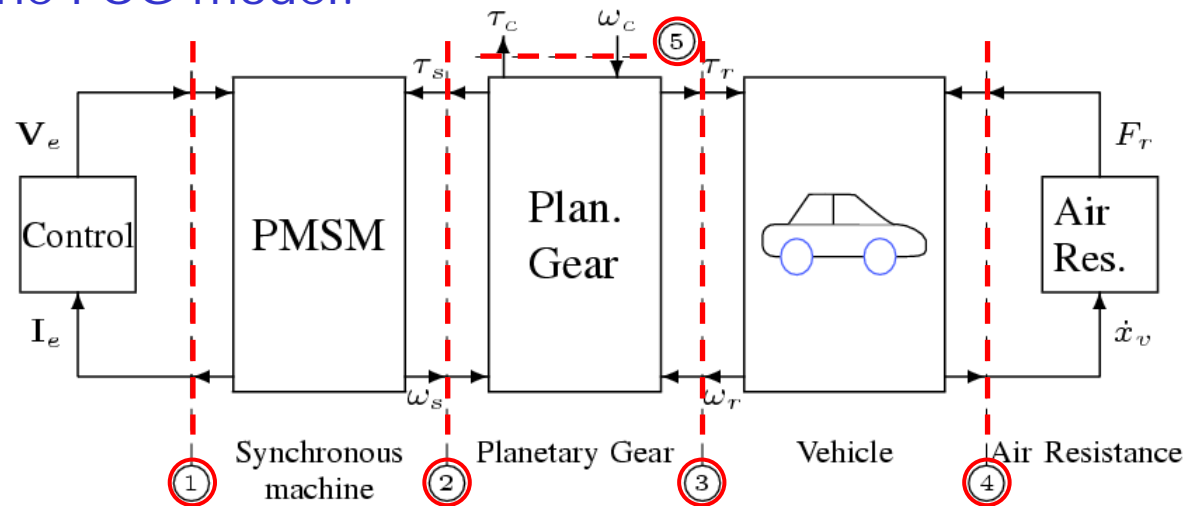
- ICE
- PMSM
- vehicle

With the POG technique *it is easy to connect the subsystems* because it is based on the use of the “dashed” power sections!

The system:

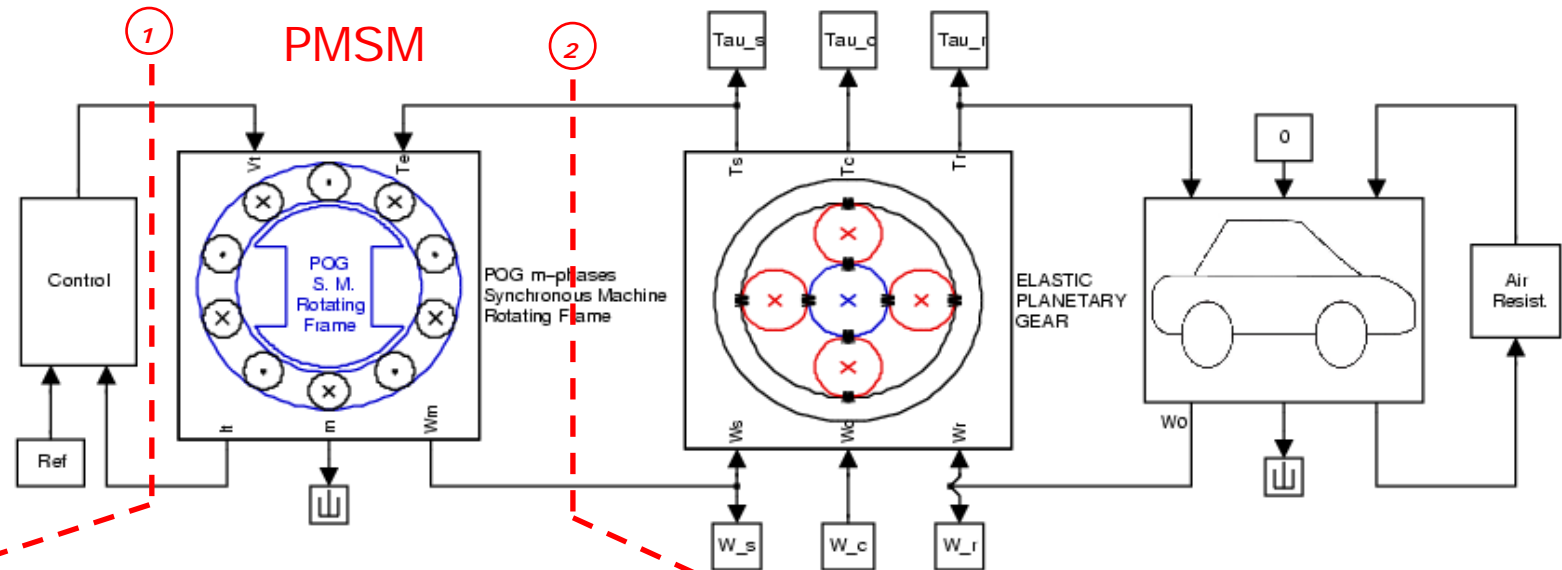


The POG model:

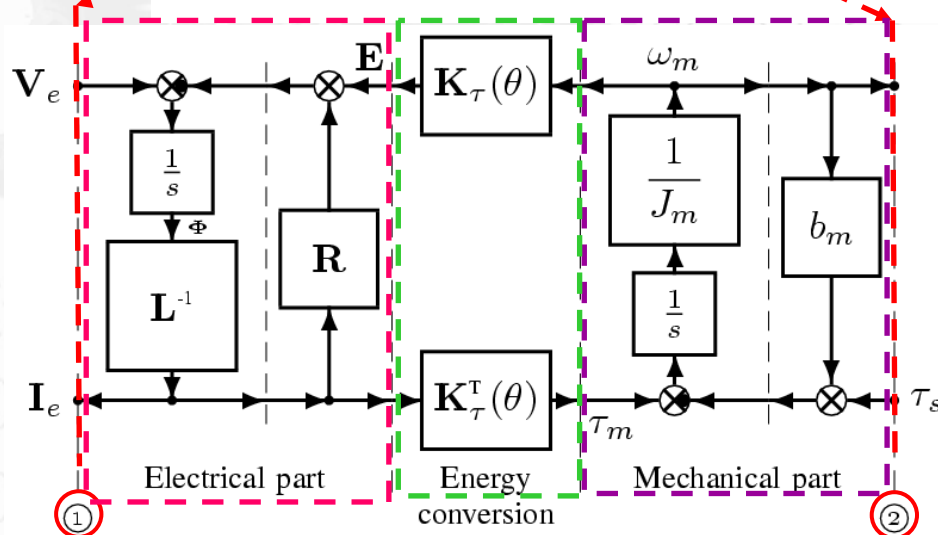


# Hybrid Automotive Systems: POG model

The Simulink block scheme:



POG model of PMSM:



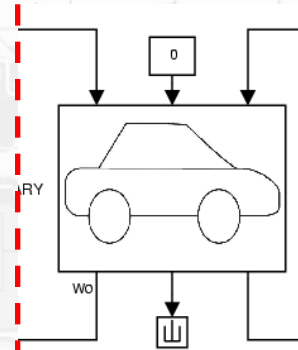
PMSM: Permanent Magnet Synchronous Motor

- Electrical part
- Mechanical part
- Energy conversion

# Hybrid Automotive Systems: POG model

## POG model of the vehicle:

- From transmission to center of mass
- Mechanical dynamics
- From center of mass to road contact

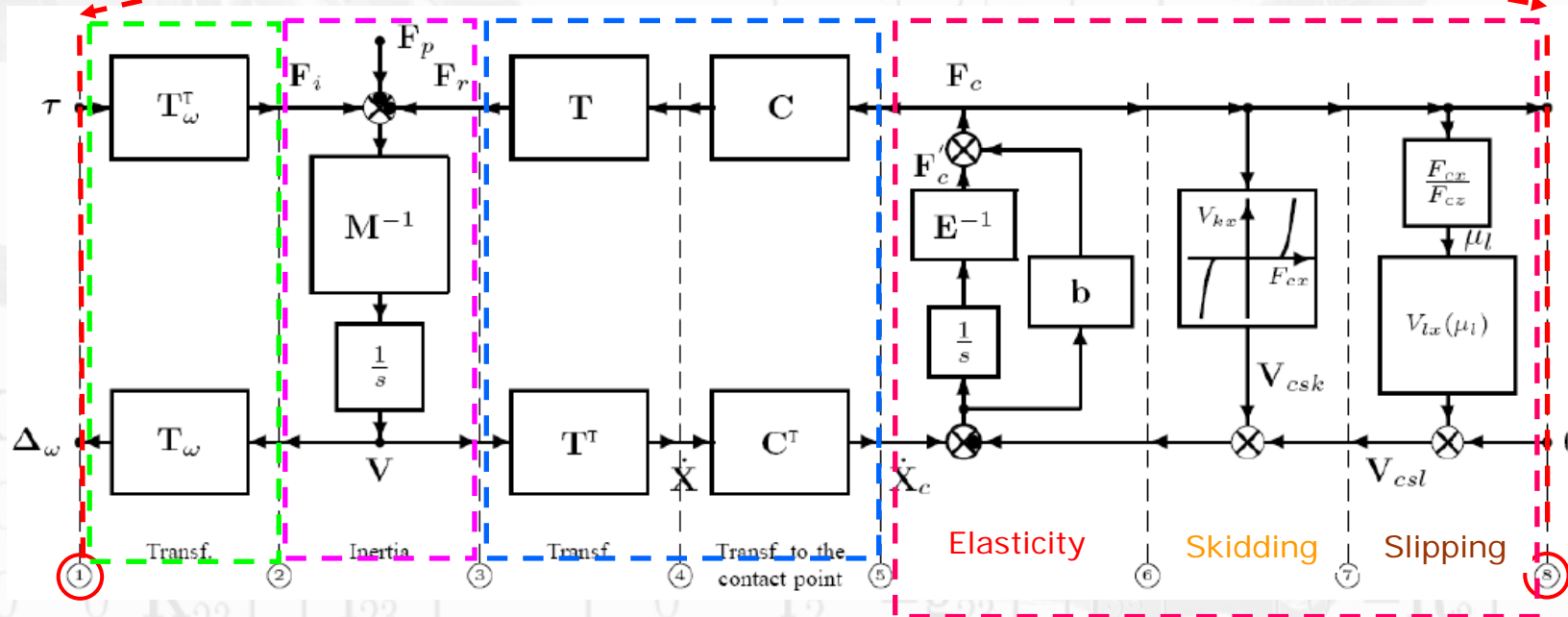


-- Tire-road contact:

Elasticity

Skidding

Slipping



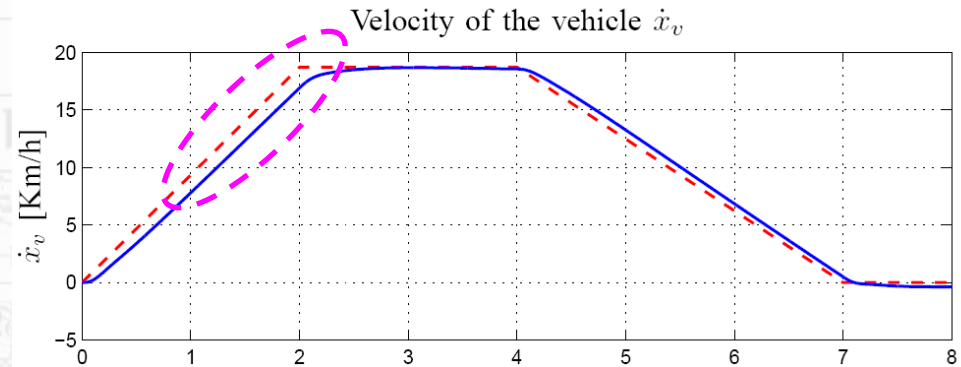
# Hybrid Automotive Systems: simulations

“Start and stop” simulation results obtained with the ICE switched off:

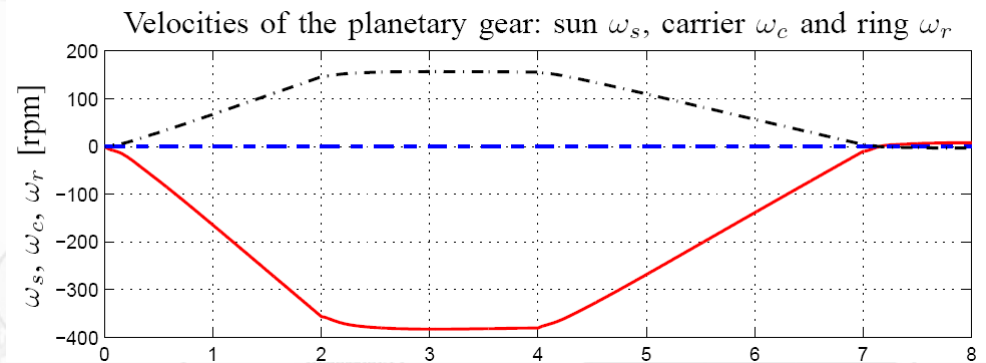
$$\omega_c = 0$$

The small tracking delay is due to the elastic horizontal slipping of the tires on the ground.

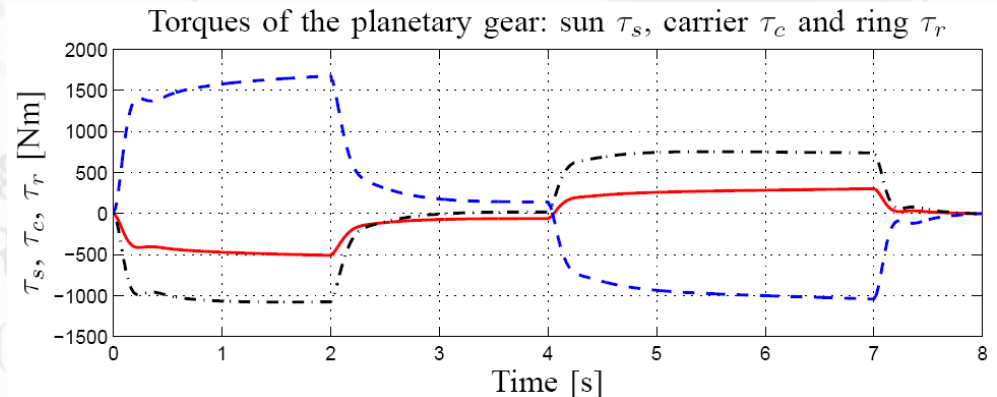
Vehicle velocity



Planetary gear velocities



Planetary gear torques



# Hybrid Automotive Systems: simulations

A PMSM multiphase electric motor has been used:

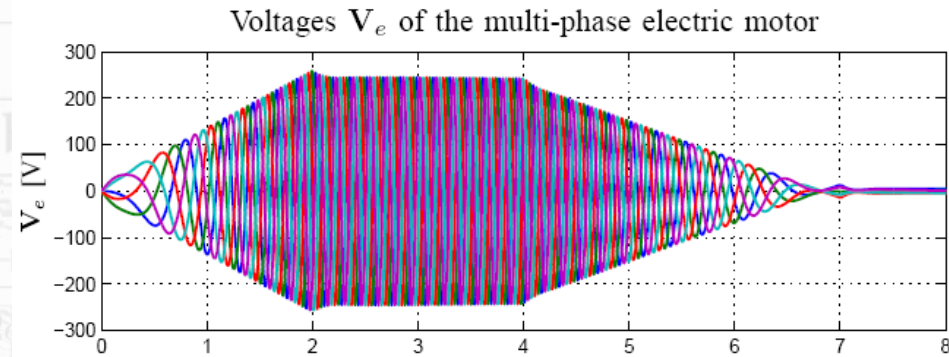
$$m = 5$$

It can be useful to improve the robustness and safety of the system

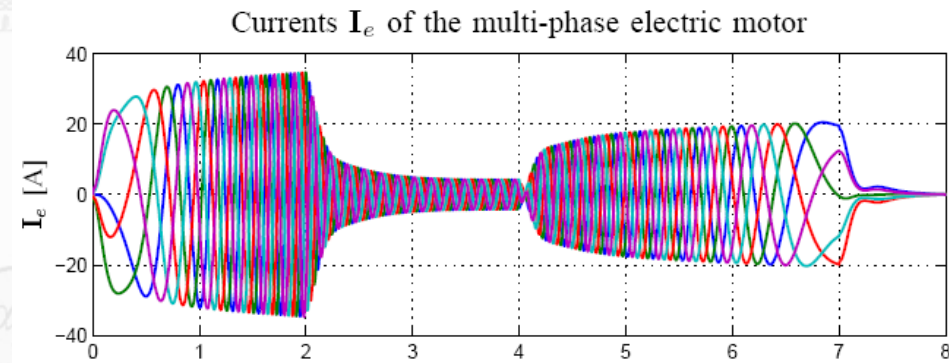
With POG models clearly shows the "power flows" within the system:

- motor
- generator

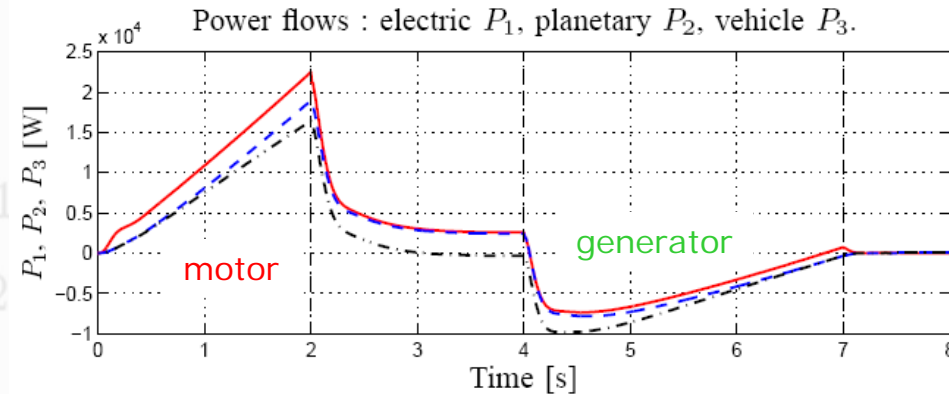
Electric motor voltages



Electric motor currents



Power flows



# Conclusions

## 1) POG modeling technique:

- a planetary gear has been modeled with different level of details (reduction rules),
- an hybrid automotive power system (endothermic engine, multi-phase synchronous motor, planetary gear and vehicle dynamics) has been modeled.

## 2) The POG technique is **easy to use, easy to understand and suitable for modeling complex dynamic systems** such as Hybrid Automotive Systems