

Modeling of Automotive Control Systems Using Power Oriented Graphs



UNIVERSITÀ DEGLI STUDI
DI MODENA E REGGIO EMILIA

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$$\begin{bmatrix} K_{12}^{-1} & 0 & 0 \\ 0 & J_2 & 0 \\ 0 & 0 & K_{23}^{-1} \end{bmatrix} \begin{bmatrix} \dot{f}_{12} \\ \dot{\omega}_2 \\ \dot{f}_{23} \end{bmatrix} = \begin{bmatrix} -g_{12} & -R_2^T & 0 \\ R_2 & -b_2 & -r_3^T \\ 0 & r_2 & -g_{23} \end{bmatrix} \begin{bmatrix} f_{12} \\ \omega_2 \\ f_{23} \end{bmatrix} + \begin{bmatrix} r_1 & 0 \\ 0 & 0 \\ -R_3^T \end{bmatrix} \begin{bmatrix} v_{1i} \\ v_{2i} \\ v_{3e} \end{bmatrix}$$

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Outline

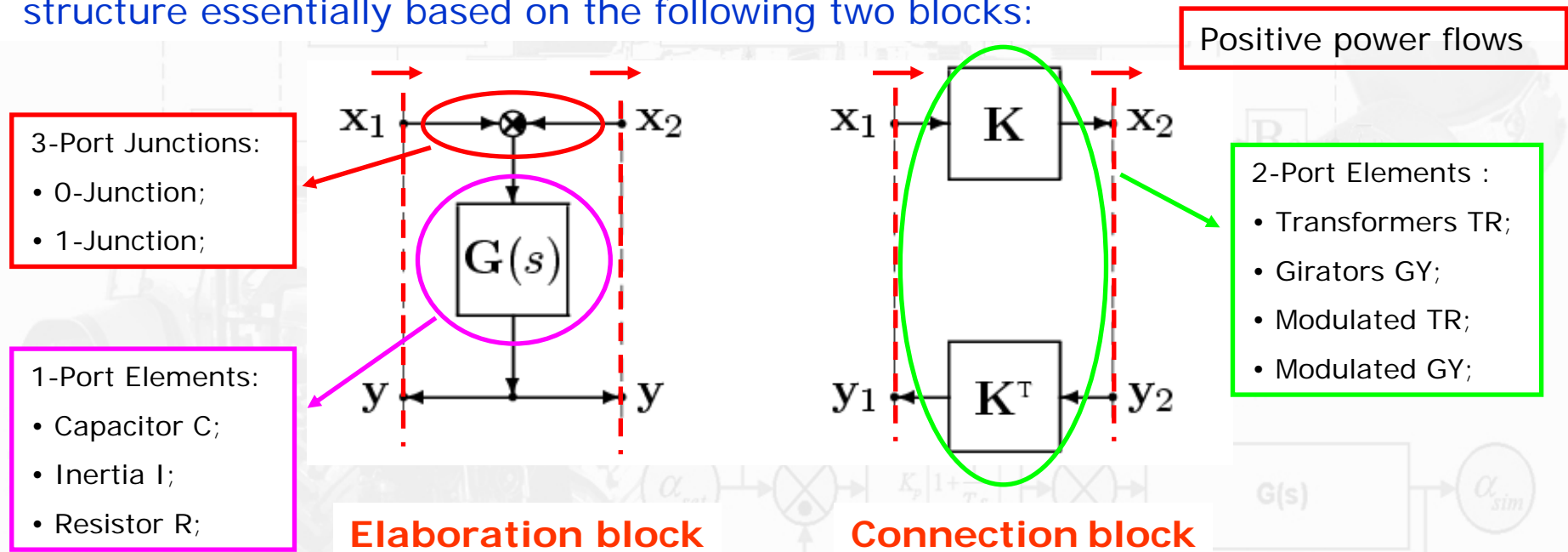
- Introduction on Power-Oriented Graphs (POG)
- POG and Port-Controlled Hamiltonian (PCH) systems
- Modified PCH: introduction of “direct dissipations”
- Example: Clutch Control System

- Conclusions

Introduction

Power-Oriented Graphs (POG)

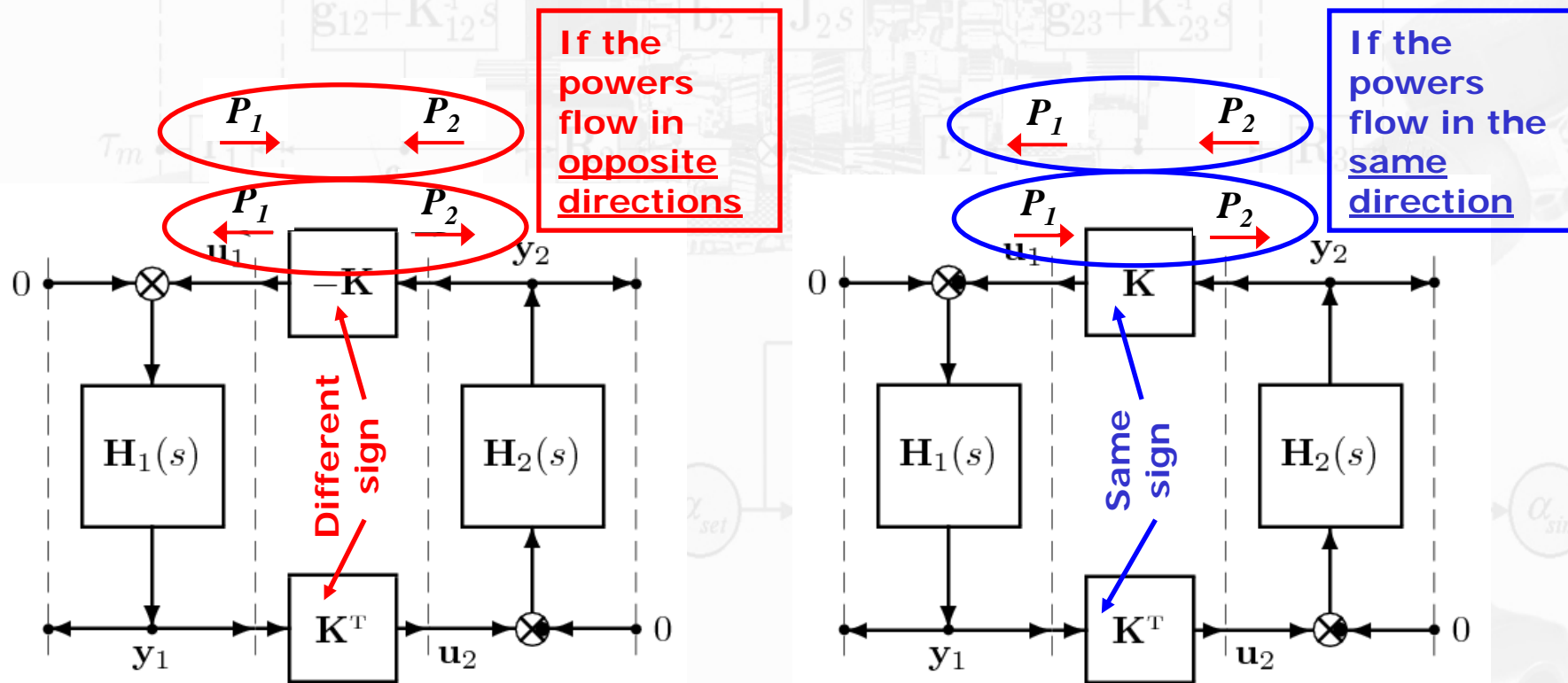
The Power-Oriented Graphs are "block diagrams" obtained by using a "modular" structure essentially based on the following two blocks:



- POG maintains a direct correspondence between pairs of system variables and real power flows: the product of the two variables involved in each dashed line of the graph has the physical meaning of "power flowing through that section".
- The Elaboration block can store and dissipate/generate energy.
- The Connection block can only "transform" the energy.

POG Dynamic Modeling: Connection blocks

In the general vector case the connection block is characterized by a matrix K .



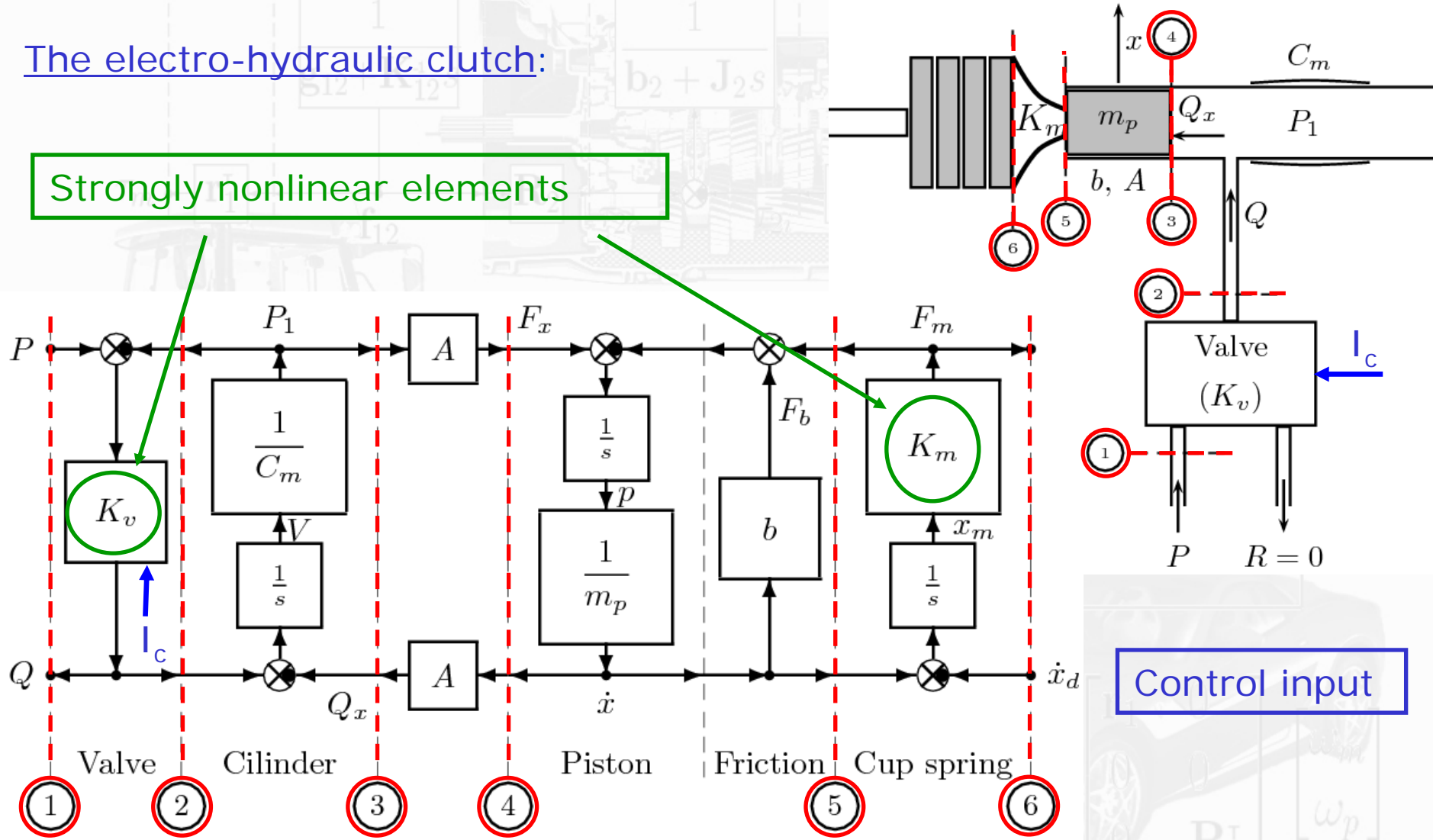
Matrix K is rectangular if systems $H_1(s)$ and $H_2(s)$ have different dimensions.

Matrix $K=K(x, v)$ that can also be a function of state variables x or external variables v .

Example of POG modeling: an electro-hydraulic clutch

The electro-hydraulic clutch:

Strongly nonlinear elements



Dynamic Modeling of Physical Systems

Different Energy domains:

1) Electrical; 2) Mechanical (tras./rot.); 3) Hydraulic; **etc.**

The same dynamic structure:

- 2 “dynamic” elements D_1, D_2 that store energy;
- 1 “static” element R that dissipates (or generates) energy;
- 2 “energy variables” $q_1(t), q_2(t)$ used for describing the stored energy;
- 2 “power variables” $v_1(t), v_2(t)$ used for moving the energy;

	Electrical	Mechanical	Hydraulic
\mathcal{D}_1	C Capacitor	M Mass	C_I Hyd. Capacitor
q_1	Q Charge	p Momentum	V Volume
Across-variables	v_1 V Voltage	v Velocity	P Pressure
\mathcal{D}_2	L Inductor	E Spring	L_I Hyd. Inductor
q_2	ϕ Flux	x Displacement	ϕ_I Hyd. Flux
Through-variables	v_2 I Current	F Force	Q Flow
\mathcal{R}	R Resistor	b Friction	R_I Hyd. Resistor

In POG the new symbols and the new definitions are “minimal”

Introduction

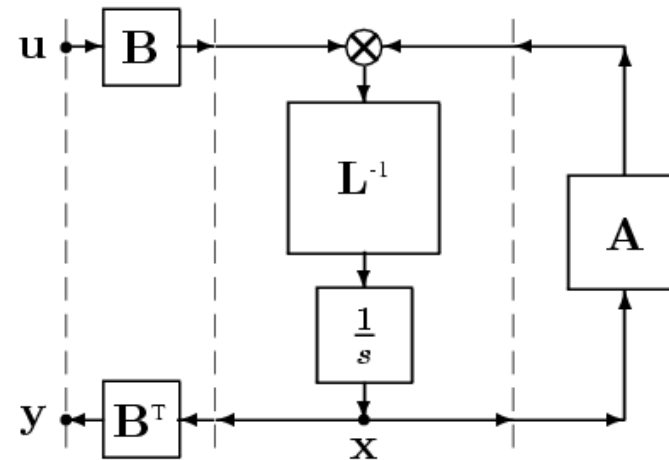
Power-Oriented Graphs - LTI Systems

- The POG are suitable for representing both scalar and vectorial systems.
- A direct correspondence between POG and state space descriptions:

$$\begin{cases} \mathbf{L}\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u} \\ \mathbf{y} = \mathbf{B}^T\mathbf{x} \end{cases}$$

Stored Energy: $E_s = \frac{1}{2}\mathbf{x}^T\mathbf{L}\mathbf{x}$

Dissipating Power: $P_d = \mathbf{x}^T\mathbf{A}\mathbf{x}$



- When an eigenvalue of matrix \mathbf{L} goes to zero (or to infinity), the system degenerates towards a lower dynamic dimension system. The “reduced” can be obtained by using “congruent” transformation $\mathbf{x}=\mathbf{T}\mathbf{z}$ (matrix \mathbf{T} is constant and it can be rectangular):

$$\begin{cases} \mathbf{T}^T\mathbf{L}\mathbf{T}\dot{\mathbf{z}} = \mathbf{T}^T\mathbf{A}\mathbf{T}\mathbf{z} + \mathbf{T}^T\mathbf{B}\mathbf{u} \\ \mathbf{y} = \mathbf{B}^T\mathbf{T}\mathbf{z} \end{cases} \Leftrightarrow \begin{cases} \bar{\mathbf{L}}\dot{\mathbf{z}} = \bar{\mathbf{A}}\mathbf{z} + \bar{\mathbf{B}}\mathbf{u} \\ \mathbf{y} = \bar{\mathbf{B}}^T\mathbf{z} \end{cases}$$

Drawback: the POG graphical schemes are not so compact as in Bond Graphs

Port-Controlled Hamiltonian Systems

Interconnection of subsystems

Many PCH can be obtained connecting different subsystems. The general form of the power preserving interconnection element is:

$$\begin{bmatrix} u_1 \\ u_2 \end{bmatrix} = \begin{bmatrix} 0 & A \\ -A^T & 0 \end{bmatrix} \begin{bmatrix} y_1 \\ y_2 \end{bmatrix}$$

Matrix **A** can also be time varying and/or state dependent.

Standard PCH cannot describe systems with a direct dissipation between the input **u** and the output **y**. A resistor is the simplest example.

Extended definition for PCH with "direct dissipation" and "direct interconnection":

$$\begin{cases} \dot{x} = [J_1(x, v) - R_1(x, v)] \frac{\partial H}{\partial x}(x) + g(x, v) u \\ y = g^T(x, v) \frac{\partial H}{\partial x}(x) + [R_2(x, v) - J_2(x, v)] u \end{cases}$$

direct interconnections

$$J_i(x, v) = -J_i^T(x, v), \quad R_i(x, v) = R_i^T(x, v) \geq 0$$

direct dissipations

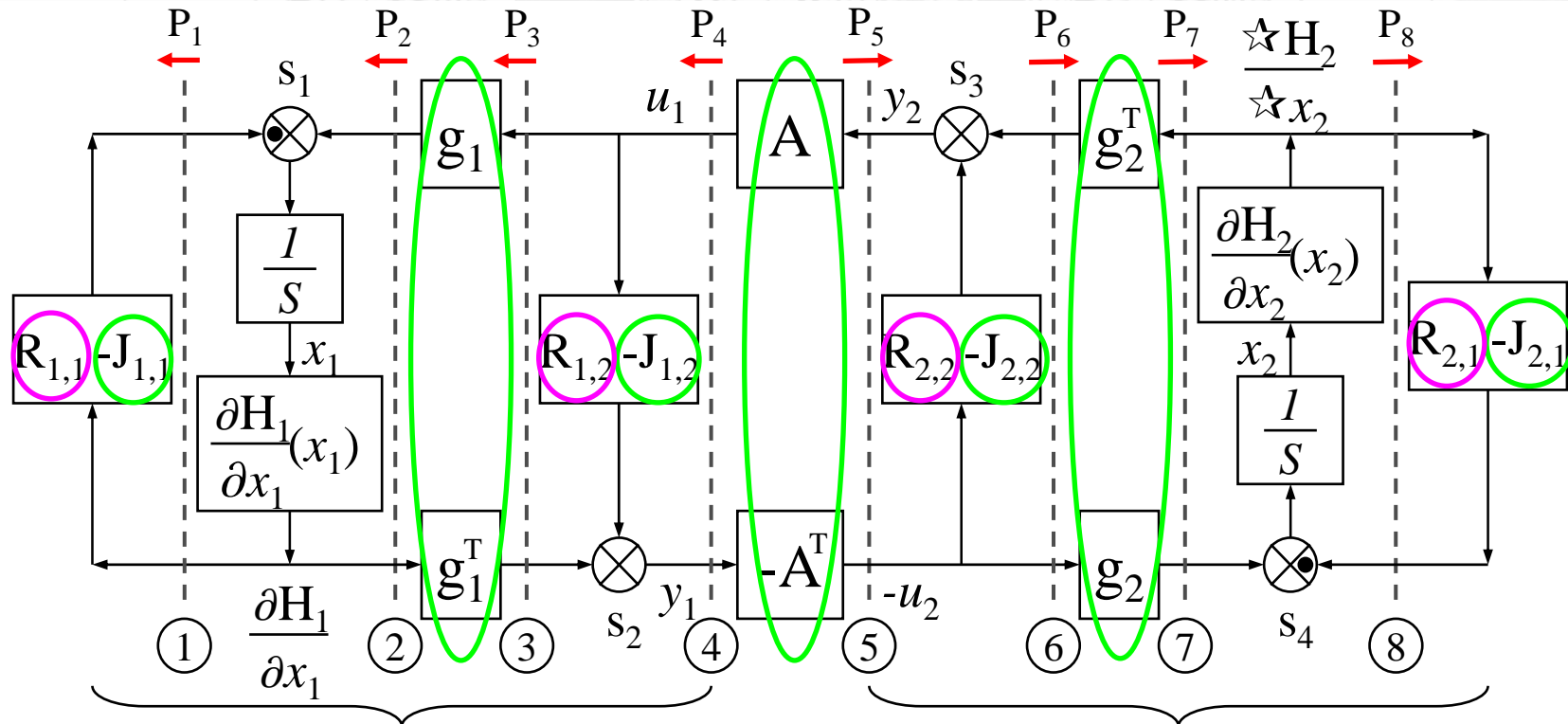
Power balance:

$$\frac{dH}{dt} = y^T u - \frac{\partial H^T}{\partial x} R_1(x, v) \frac{\partial H}{\partial x} - u^T R_2(x, v) u$$

Interconnected Systems

Relation between POG and PCH

The POG representation of two interconnected PCH:



Subsystem 1

Subsystem 2

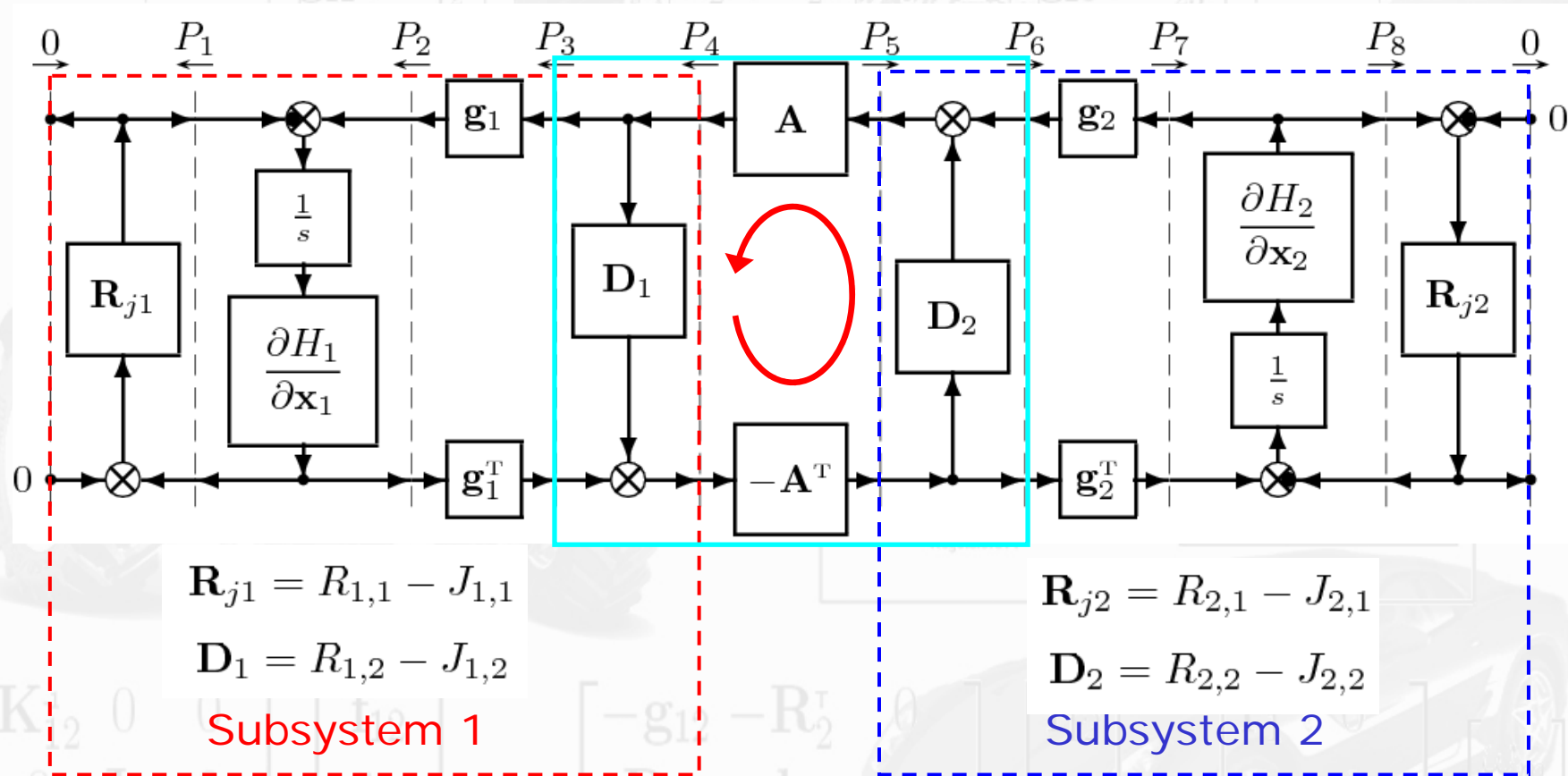
Dissipations

Connections

Interconnected Systems

Relation between POG and PCH

The POG representation of two interconnected PCH:

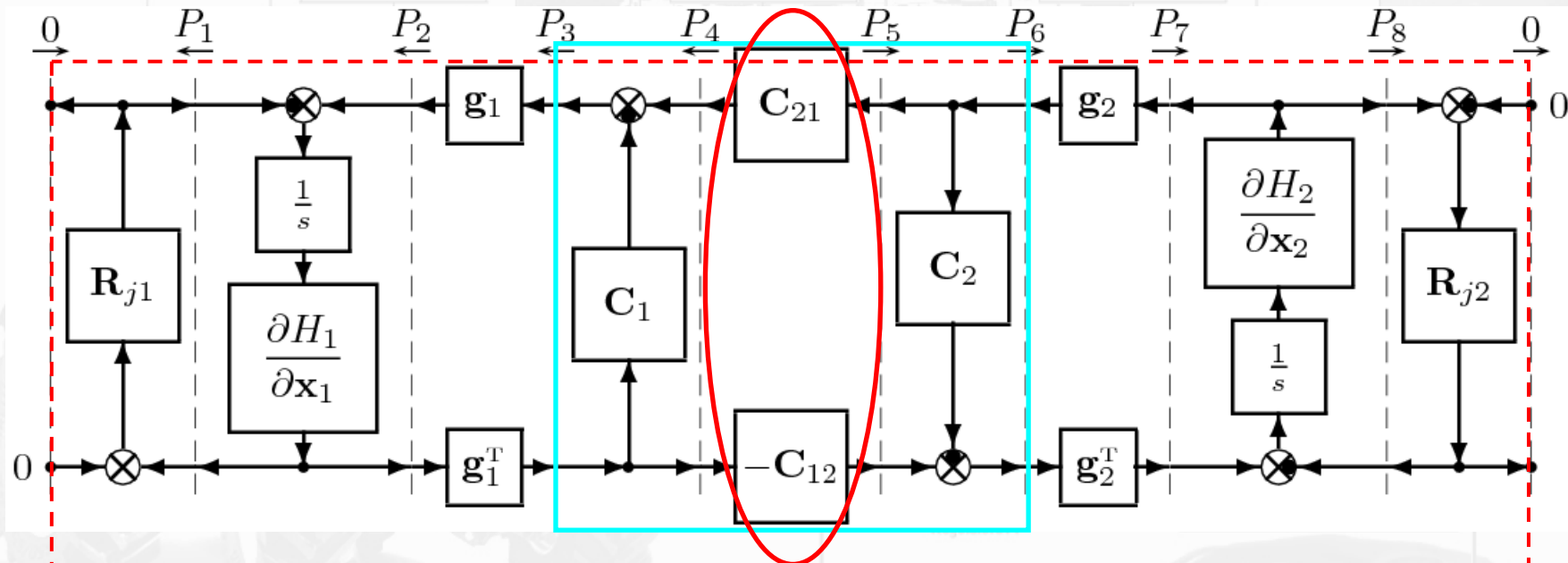


Note: in the center of the block scheme is present an algebraic loop

Interconnected Systems

Relation between POG and PCH

The POG representation of two interconnected PCH without algebraic loop:



$$C_1 = (I + AD_2A^TD_1)^{-1}AD_2A^T$$

$$C_{12} = (I + A^TD_1AD_2)^{-1}A^T$$

$$C_2 = (I + A^TD_1AD_2)^{-1}A^TD_1A$$

$$C_{21} = (I + AD_2A^TD_1)^{-1}A$$

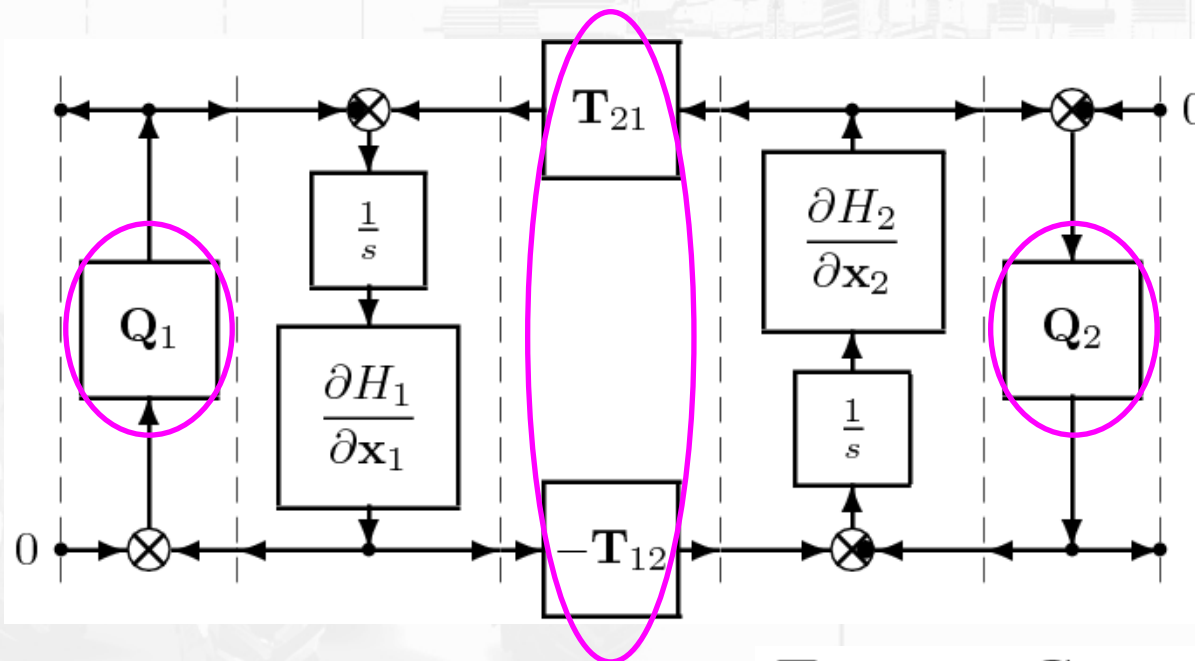
In general, it is NOT a connection block

$$C_{21} \neq C_{21}^T$$

Interconnected Systems

Relation between POG and PCH

Two interconnected PCH: the POG reduced system



$$Q_1 = R_{j1} + g_1 C_1 g_1^T$$

$$Q_2 = R_{j2} + g_2 C_2 g_2^T$$

$$T_{21} = g_1 C_{21} g_2$$

$$T_{12} = g_2^T C_{12} g_1^T$$

Subsystem 1 + Subsystem 2

POG and PCH Interconnected Systems

Example of three connected electric circuits

The RLR circuit:

$$\dot{\varphi} = [-r_{1,1}] \frac{\partial H_1}{\partial \varphi} + [1 \quad -1] \begin{bmatrix} V_{i1} \\ V_{i2} \end{bmatrix}$$

$$\begin{bmatrix} I_{o1} \\ I_{o2} \end{bmatrix} = \begin{bmatrix} 1 \\ -1 \end{bmatrix} \frac{\partial H_1}{\partial \varphi} + R_{1,2} \begin{bmatrix} V_{i1} \\ V_{i2} \end{bmatrix}$$

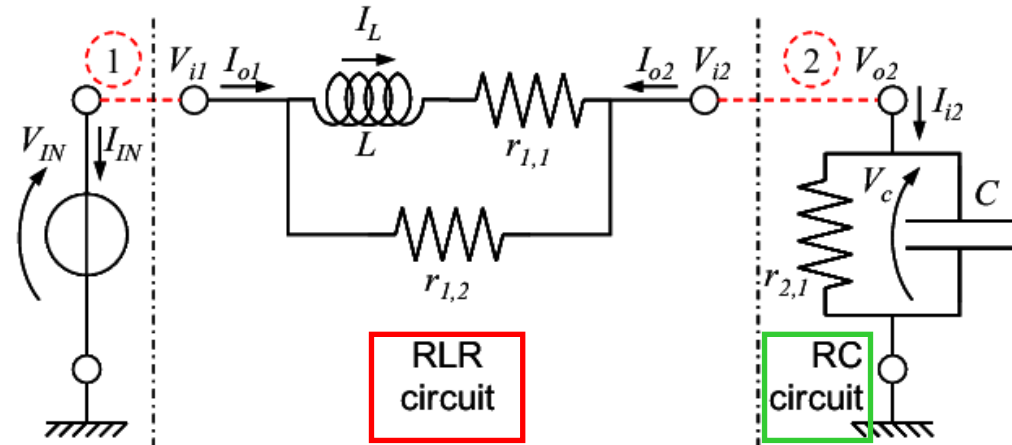
Matrix $R_{1,2}$:

$$R_{1,2} = \begin{bmatrix} 1/r_{1,2} & -1/r_{1,2} \\ -1/r_{1,2} & 1/r_{1,2} \end{bmatrix}$$

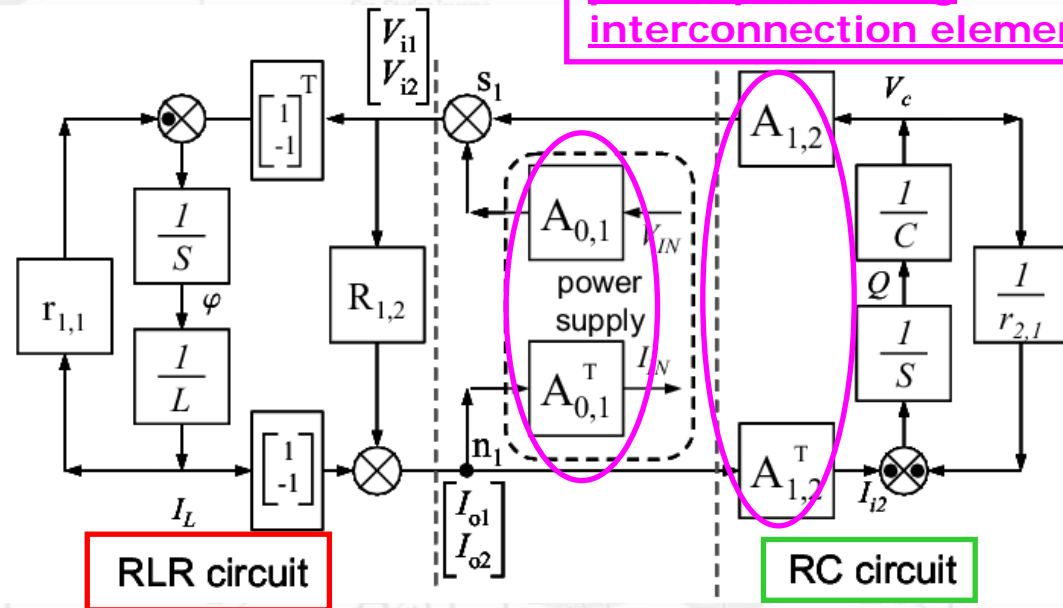
The RC circuit:

$$\dot{Q} = \begin{bmatrix} -1 \\ r_{2,1} \end{bmatrix} \frac{\partial H_2}{\partial Q} + I_{i,2}$$

$$V_{o2} = \frac{\partial H_2}{\partial Q} = V_c$$

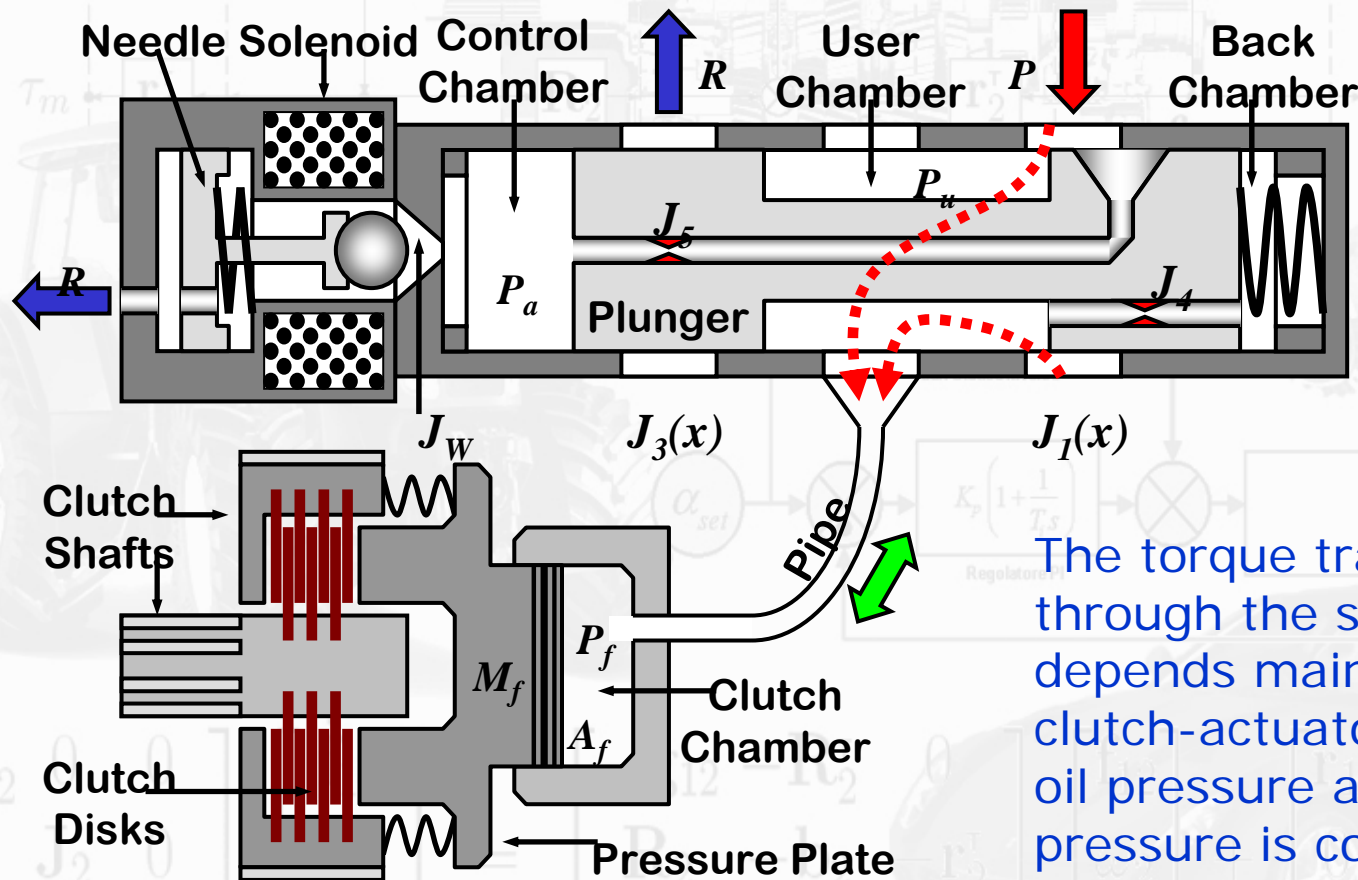


power preserving interconnection element



Application example: Electro-hydraulic clutch actuator

A simplified scheme of an Electro-hydraulic clutch actuator:



The torque transmitted through the shafts depends mainly on the clutch-actuator internal oil pressure and this pressure is controlled by the electro-valve.

Electro-hydraulic clutch actuator: the POG model

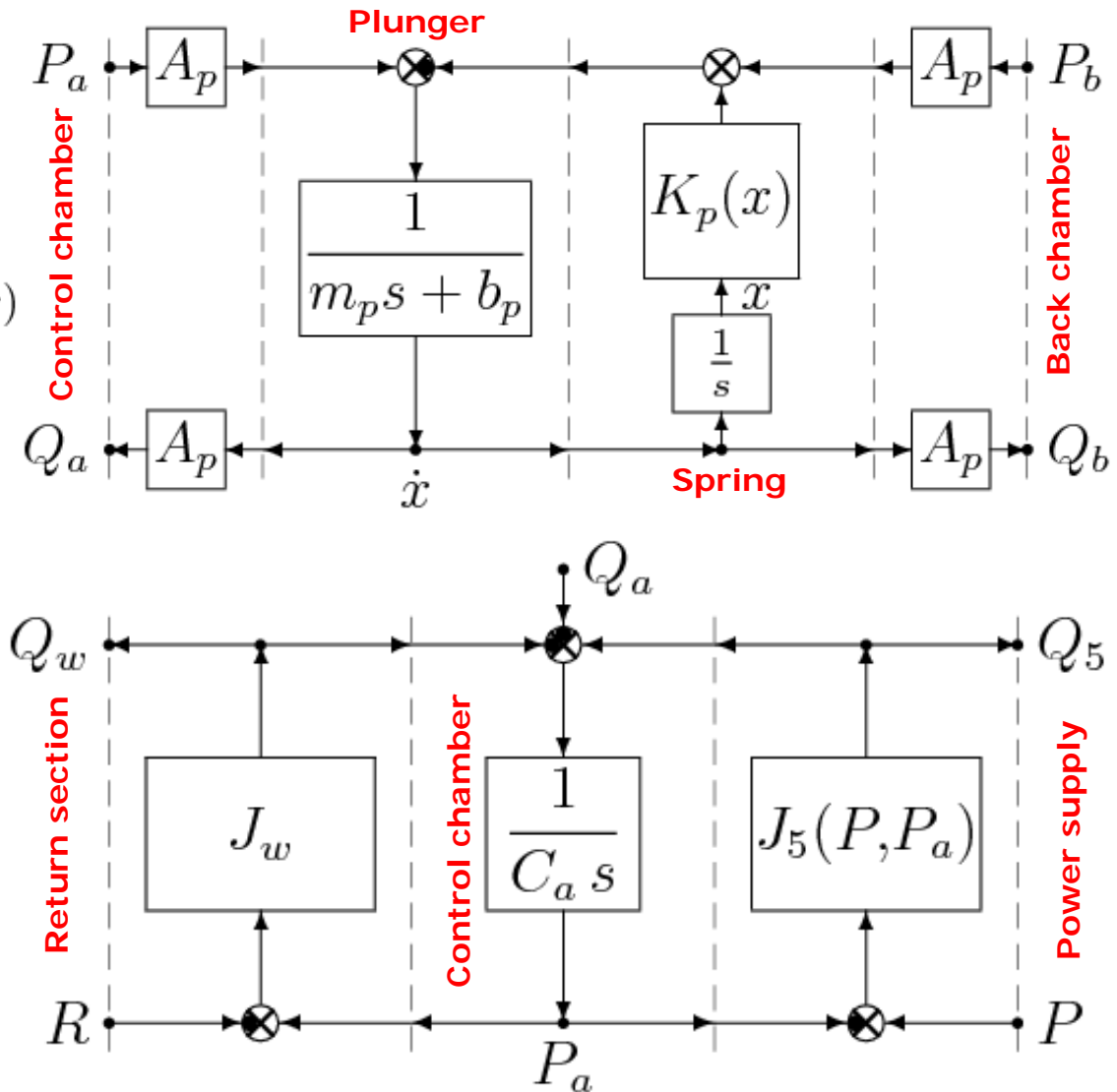
POG model of the valve plunger:

$$m_p \ddot{x} = (P_a - P_b) A_p - b_p \dot{x} - K_p(x)$$

$$Q_a = Q_b = A_p \dot{x}$$

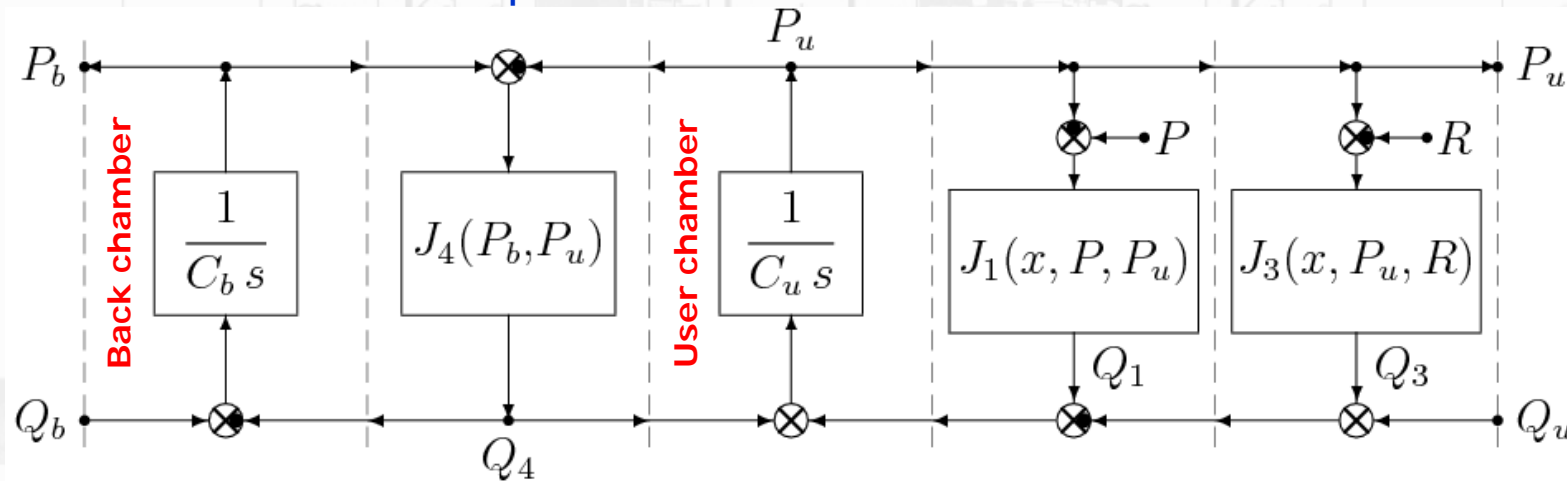
POG model of the control chamber:

$$C_a \dot{P}_a = Q_5 - Q_a - Q_w$$

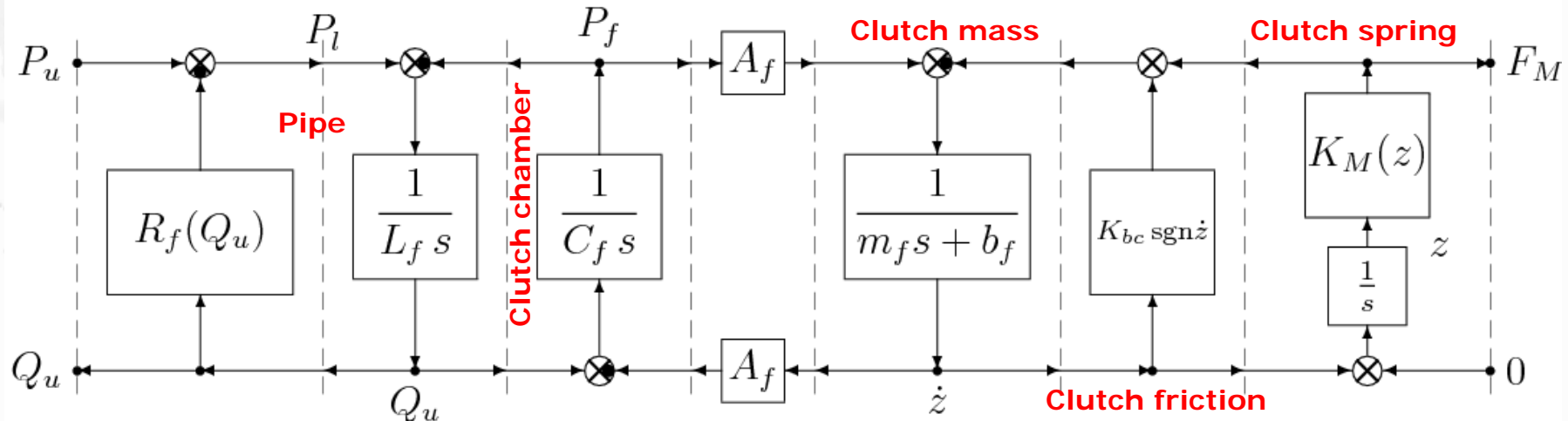


Electro-hydraulic clutch actuator: The POG model

Back chamber and output user chamber POG models:



Clutch actuator POG model:



Electro-hydraulic clutch actuator: Simulation and experimental results (1/2)

Step input measurements.

Supply pressure P (dotted)

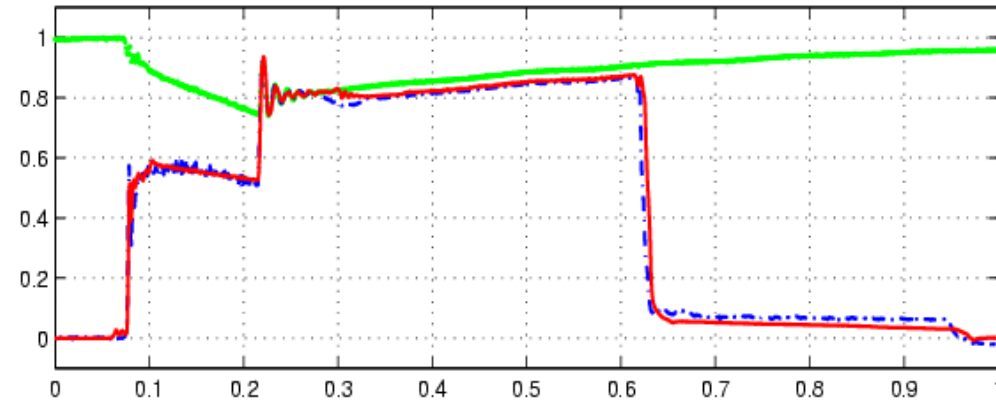
Clutch chamber pressure P_f :

- measured (dash-dotted)
- simulated (solid)

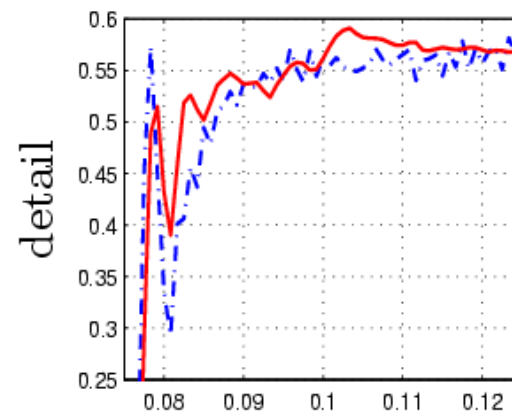
Electrovalves:



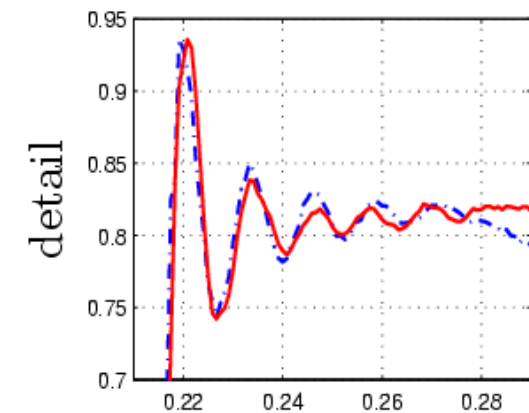
Measured $P_f(-)$, $P(.)$ Simulated $P_f(-)$



Normalized time



Normalized time

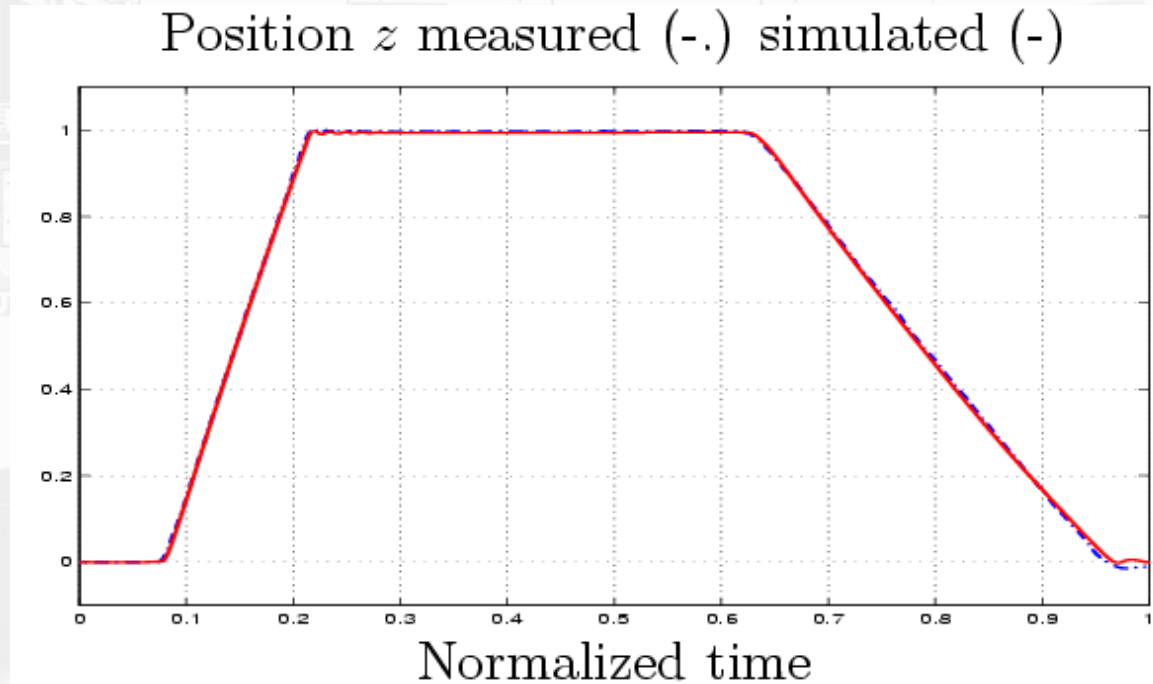


Normalized time

Electro-hydraulic clutch actuator: Simulation and experimental results (2/2)

Clutch actuator position z :

- measured (dash-dotted)
- simulated (solid)



The figure axes are normalized.

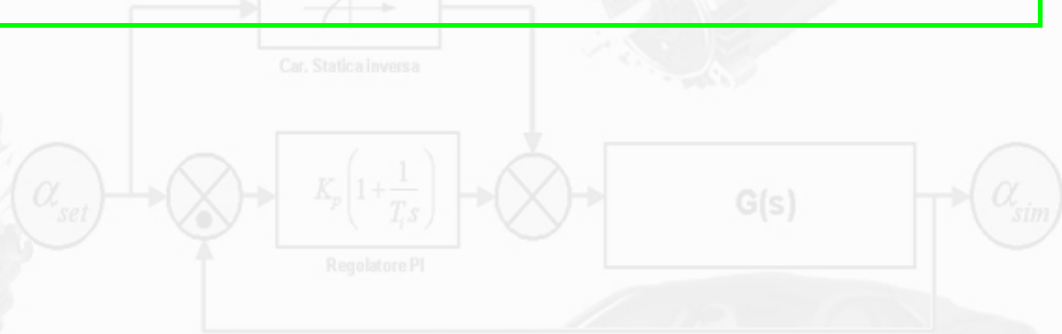
The simulations are very similar to the experimental data proving that the modeling approach is suitable to this kind of multi-domain systems.

Conclusions

- The paper has addressed the problem of modeling physical systems by using the Power-Oriented Graphs (POG) modeling technique.
- The Port-Controlled Hamiltonian (PCH) systems has been graphically described by using the POG modeling technique.
- A slight extension of the definition of PCH has been given introducing the “direct dissipations” and “direct connections”.
- The POG technique has been used for modeling a clutch control system. The obtained simulation results are very similar to the experimental data.



Thank you for your attention!



$$\begin{bmatrix} K_{12}^{-1} & 0 & 0 \\ 0 & J_2 & 0 \\ 0 & 0 & K_{23}^{-1} \end{bmatrix} \begin{bmatrix} \dot{f}_{12} \\ \dot{\omega}_2 \\ \dot{f}_{23} \end{bmatrix} = \begin{bmatrix} -g_{12} & -R_2^T & 0 \\ R_2 & -b_2 & -r_2^T \\ 0 & r_2 & -g_{23} \end{bmatrix} \begin{bmatrix} f_{12} \\ \omega_2 \\ f_{23} \end{bmatrix} + \begin{bmatrix} r_1 & 0 \\ 0 & 0 \\ -R_3^T \end{bmatrix} \begin{bmatrix} v_{1i} \\ v_{2i} \\ \omega_p \end{bmatrix}$$