

**System and Control Theory**  
**Test of January 23, 2013**  
**Questions and Exercises**

Name:	
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Signature:	

1. Write the discrete time behavior of the output function  $\mathbf{y}(k)$ , solution of the difference equation  $\mathbf{x}(k+1) = \mathbf{A}\mathbf{x}(k) + \mathbf{B}\mathbf{u}(k)$  and the static equation  $\mathbf{y}(k) = \mathbf{C}\mathbf{x}(k) + \mathbf{D}\mathbf{u}(k)$  starting from the initial condition  $\mathbf{x}(h)$  at time  $h$ :

$$\mathbf{y}(k) = \mathbf{C}\mathbf{A}^{k-h}\mathbf{x}(h) + \mathbf{C}\sum_{j=h}^{k-1}\mathbf{A}^{k-j-1}\mathbf{B}\mathbf{u}(j) + \mathbf{D}\mathbf{u}(k)$$

2. Write the general solution of the following time-varying differential equation  $\dot{\mathbf{x}} = \mathbf{A}(t)\mathbf{x}(t) + \mathbf{B}(t)\mathbf{u}(t)$ , being  $\mathbf{x}(t_0)$  the state at time  $t_0$ :

$$\mathbf{x}(t) = \Phi(t, t_0)\mathbf{x}(t_0) + \int_{t_0}^t \Phi(t, \tau)\mathbf{B}(\tau)\mathbf{u}(\tau)d\tau$$

where  $\Phi(t, \tau)$  is the state transition matrix of the system in the time interval  $[\tau, t]$ .

3. Compute the reachability matrix  $\mathcal{R}^+$  and the observability matrix  $\mathcal{O}^-$  of the following system:

$$\begin{cases} \dot{\mathbf{x}}(t) = \begin{bmatrix} -1 & 0 & -2 \\ 2 & 1 & 2 \\ 0 & 0 & 1 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 1 \\ -1 \\ 1 \end{bmatrix} u(t) \\ y(t) = [0 \quad 1 \quad -1] \mathbf{x}(t) \end{cases} \quad \mathcal{R}^+ = \begin{bmatrix} 1 & -3 & 1 \\ -1 & 3 & -1 \\ 1 & 1 & 1 \end{bmatrix}, \quad \mathcal{O}^- = \begin{bmatrix} 0 & 1 & -1 \\ 2 & 1 & 1 \\ 0 & 1 & -1 \end{bmatrix}$$

The system is:  reachable?  not-reachable?  observable?  not-observable?

Provide a base of the reachable subspace  $\mathcal{X}^+$  and a base of the not-observable subspace  $\mathcal{E}^-$ :

$$\mathcal{X}^+ = \text{Im} \begin{bmatrix} 1 & -3 \\ -1 & 3 \\ 1 & 1 \end{bmatrix}, \quad \mathcal{E}^- = \text{Im} \begin{bmatrix} -1 \\ 1 \\ 1 \end{bmatrix}.$$

4. Write the definition of the characteristic polynomial  $\Delta_{\mathbf{A}}(\lambda)$  of a matrix  $\mathbf{A} \in \mathbf{R}^{n \times n}$ :

$$\Delta_{\mathbf{A}}(\lambda) = \det(\lambda\mathbf{I} - \mathbf{A})$$

The roots of the characteristic polynomial:

- are the eigenvalues of matrix  $\mathbf{A}$ ;  always have multiplicity equal to 1;  
 are eigenvectors of matrix  $\mathbf{A}$ ;  always are in a number equal to  $n$ ;  
 can be complex conjugate;  always are real;

5. Given a continuous-time linear system:  $\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t)$  and  $\mathbf{y}(t) = \mathbf{C}\mathbf{x}(t) + \mathbf{D}\mathbf{u}(t)$ . Apply the Laplace transform to the system and provide the expression of the transform  $\mathbf{y}(s)$  of the output vector  $\mathbf{y}(t)$  corresponding to the *forced evolution* of the system:

$$\mathbf{y}(s) = [\mathbf{C}(s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B} + \mathbf{D}]\mathbf{u}(z)$$

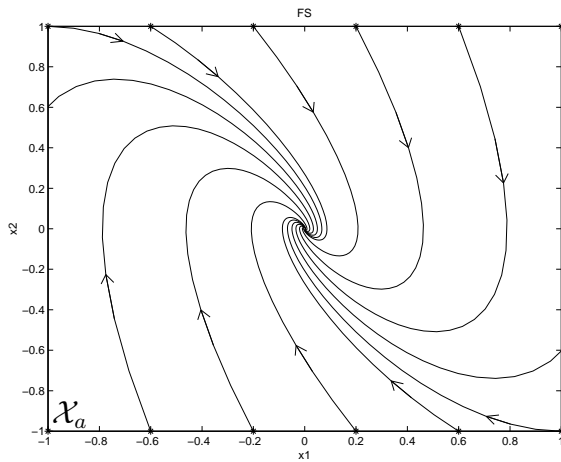
6. Given an autonomous system  $\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t)$  of the fourth order where the matrix  $\mathbf{A}$  can be given the “real” Jordan form  $\mathbf{A}_R = \mathbf{T}_R^{-1}\mathbf{A}\mathbf{T}_R$  using the state space transformation  $\mathbf{x} = \mathbf{T}_R\bar{\mathbf{x}}$ :

$$\mathbf{A} = \begin{bmatrix} 1 & 1 & 0 & 2 \\ 0.4 & -2.2 & 0.4 & 1.6 \\ -4 & -2 & -3 & -4 \\ 0.8 & 0.6 & 0.8 & -1.8 \end{bmatrix}, \quad \mathbf{A}_R = \begin{bmatrix} -2 & -1 & 0 & 0 \\ 1 & -2 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & -3 \end{bmatrix}, \quad \mathbf{T}_R = \begin{bmatrix} -1 & 0 & -1 & 0 \\ 1 & 1 & 0 & -2 \\ 0 & -2 & 1 & 0 \\ 1 & 0 & 0 & 1 \end{bmatrix}$$

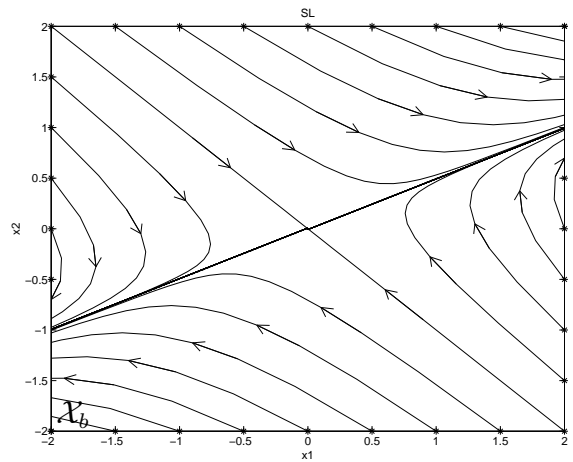
- a) Write the eigenvalues  $\lambda_i$  and the eigenvectors  $\mathbf{v}_i$  that characterize the matrix  $\mathbf{A}$ :

$$\begin{aligned} \lambda_1 &= -2+j \\ \lambda_2 &= -2-j \\ \lambda_3 &= 1 \\ \lambda_4 &= -3 \end{aligned} \quad \mathbf{v}_1 = \begin{bmatrix} -1 \\ 1+j \\ -2j \\ 1 \end{bmatrix}, \quad \mathbf{v}_2 = \begin{bmatrix} -1 \\ 1-j \\ 2j \\ 1 \end{bmatrix}, \quad \mathbf{v}_3 = \begin{bmatrix} -1 \\ 0 \\ 1 \\ 0 \end{bmatrix}, \quad \mathbf{v}_4 = \begin{bmatrix} 0 \\ -2 \\ 0 \\ 1 \end{bmatrix}.$$

b.1) Draw qualitatively the trajectories generated in the plane  $\mathcal{X}_a$  by the two complex conjugate eigenvalues of the dynamic system:



b.2) Draw qualitatively the trajectories generated in the plane  $\mathcal{X}_b$  by the two real eigenvalues of the dynamic system:



c.1) Write the type of trajectories:

- Node?     Focus?     Saddle?  
 Stable?     Unstable?

c.2) Write the type of trajectories:

- Node?     Focus?     Saddle?  
 Stable?     Unstable?

d.1) Provide a base  $\mathcal{B}_a$  of plane  $\mathcal{X}_a = \text{Im}\mathcal{B}_a$ :

$$\mathcal{B}_a = \begin{bmatrix} -1 & 0 \\ 1 & 1 \\ 0 & -2 \\ 1 & 0 \end{bmatrix}$$

d.2) Provide a base  $\mathcal{B}_b$  of plane  $\mathcal{X}_b = \text{Im}\mathcal{B}_b$ :

$$\mathcal{B}_b = \begin{bmatrix} -1 & 0 \\ 0 & -2 \\ 1 & 0 \\ 0 & 1 \end{bmatrix}$$

7. Relatively to a discrete-time linear system  $\mathbf{x}(k+1) = \mathbf{A}\mathbf{x}(k) + \mathbf{B}\mathbf{u}(k)$  that has at least an eigenvalue in the origin, it can be stated that:

- if the system is completely observable then it is also completely constructable;  
 if the system is completely constructable then it is also completely observable;  
 if the system is completely controllable then it is also completely reachable;  
 if the system is completely reachable then it is also completely controllable;

- the system can be asymptotically stable;
8. An “open loop” state estimator can be used
- if and only if the system is observable;
  - if and only if the system is asymptotically stable;
  - if and only if the unstable part of the system is observable;
  - if and only if the not-observable part of the system is asymptotically stable;
9. A system  $(\mathbf{A}, \mathbf{B}, \mathbf{C})$  is “stabilizable” using a static state feedback
- if the system is stable;
  - if the system is observable;
  - if the unstable part of the system is reachable;
  - if the part not-reachable of the system is stable;
10. The Ackermann formula for computing the vector  $\mathbf{k}^T$  allowing the free positioning of the eigenvalues of the feedback system can be used:
- for whatever system;
  - only for systems with one input;
  - only if the system is reachable;
  - also for unstable systems;

Provide the explicit description of the Ackermann formula and the desired polynomial  $p(\lambda)$  when all the  $n$  eigenvalues of the system must be located in  $\lambda = -3$ :

$$\mathbf{k}^T = - \begin{bmatrix} 0 & \dots & 0 & 1 \end{bmatrix} (\mathcal{R}^+)^{-1} p(\mathbf{A}) \quad p(\lambda) = (\lambda + 3)^n$$

11. Given a SISO linear system of the fourth order ( $n = 4$ ), completely reachable, characterized by matrices  $\mathbf{A}$ ,  $\mathbf{b}$  and  $\mathbf{c}$ .
- a) Write the structure of the matrices  $\mathbf{A}_c$ ,  $\mathbf{b}_c$  and  $\mathbf{c}_c$  of the corresponding controllability canonical form. Let  $p(\lambda) = \lambda^4 + \alpha_3 \lambda^3 + \alpha_2 \lambda^2 + \alpha_1 \lambda + \alpha_0$  the characteristic polynomial of matrix  $\mathbf{A}$ .

$$\mathbf{A}_c = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ -\alpha_0 & -\alpha_1 & -\alpha_2 & -\alpha_3 \end{bmatrix}, \quad \mathbf{b}_c = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \end{bmatrix}, \quad \mathbf{c}_c = \begin{bmatrix} \beta_0 & \beta_1 & \beta_2 & \beta_3 \end{bmatrix}$$

- b) Moreover, write the structure of matrix  $\mathbf{T}$  which, together with the space transformation  $\mathbf{x} = \mathbf{T}\mathbf{x}_c$ , brings the system in controllability canonical form.

$$\mathbf{T} = \mathcal{R}^+(\mathcal{R}_c^+)^{-1} = \begin{bmatrix} \mathbf{b} & \mathbf{A}\mathbf{b} & \mathbf{A}^2\mathbf{b} & \mathbf{A}^3\mathbf{b} \end{bmatrix} \begin{bmatrix} \alpha_1 & \alpha_2 & \alpha_3 & 1 \\ \alpha_2 & \alpha_3 & 1 & 0 \\ \alpha_3 & 1 & 0 & 0 \\ 1 & 0 & 0 & 0 \end{bmatrix}$$

12. Given the following continuous-time linear system  $\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t)$ ,  $\mathbf{y}(t) = \mathbf{C}\mathbf{x}(t)$ . Write the expression of the matrices  $\mathbf{F}$ ,  $\mathbf{G}$  and  $\mathbf{H}$  that characterize the corresponding sampled system  $\mathbf{x}(k+1) = \mathbf{F}\mathbf{x}(k) + \mathbf{G}\mathbf{u}(k)$ ,  $\mathbf{y}(k) = \mathbf{H}\mathbf{x}(k)$  with period  $T$ :

$$\mathbf{F} = e^{\mathbf{A}T}, \quad \mathbf{G} = \int_0^T e^{\mathbf{A}\sigma} \mathbf{B} d\sigma, \quad \mathbf{H} = \mathbf{C}$$

13. Write the structure of the matrix  $\mathbf{P}^{-1}$  of the state space transformation  $\mathbf{x} = \mathbf{P}\bar{\mathbf{x}}$  which brings a not-observable system in the standard observability form:

$$\mathbf{P}^{-1} = \begin{bmatrix} \mathbf{P}_1 \\ \mathbf{P}_2 \end{bmatrix} \quad \text{where} \quad \text{Im}\mathbf{P}_1^T = \text{Im}(\mathcal{O}^-)^T \text{ and } \mathbf{P}_2 \text{ makes non singular the matrix } \mathbf{P}^{-1}.$$

Moreover, write the block structure of the matrices  $\bar{\mathbf{A}}$ ,  $\bar{\mathbf{B}}$  and  $\bar{\mathbf{C}}$ :

$$\bar{\mathbf{A}} = \begin{bmatrix} \mathbf{A}_{1,1} & 0 \\ \mathbf{A}_{2,1} & \mathbf{A}_{2,2} \end{bmatrix} \quad \bar{\mathbf{B}} = \begin{bmatrix} \mathbf{B}_1 \\ \mathbf{B}_2 \end{bmatrix}$$

$$\bar{\mathbf{C}} = [ \mathbf{C}_1 \quad 0 ]$$

Write the simplified form of transfer matrix  $\mathbf{H}(s)$  of the system  $\mathcal{S}$  as a function of the sub-matrices  $\mathbf{A}_{i,j}$ ,  $\mathbf{B}_i$  and  $\mathbf{C}_j$  that characterize the system  $\bar{\mathcal{S}} = (\bar{\mathbf{A}}, \bar{\mathbf{B}}, \bar{\mathbf{C}})$ :

$$\mathbf{H}(s) = \mathbf{C}_1(s\mathbf{I} - \mathbf{A}_{11})^{-1}\mathbf{B}_1$$

14. Write the “*separation property*” of the regulator:

*The design of the feedback block  $(\mathbf{A} + \mathbf{BK})$  and the estimation block  $(\mathbf{A} + \mathbf{LC})$  can be done independently:*

$$\det[z\mathbf{I} - \bar{\mathbf{A}}] = \det[z\mathbf{I} - (\mathbf{A} + \mathbf{BK})] \det[z\mathbf{I} - (\mathbf{A} + \mathbf{LC})]$$

15. Consider the point-to-point control problem for a discrete-time linear system. Among the infinite solutions  $\mathbf{u}$  that move the system from the initial state  $\mathbf{x}(0)$  to the final state  $\mathbf{x}(k)$  in the time interval  $[0, k]$  write the structure of the solution  $\mathbf{u}$  which minimizes the Euclidean norm  $\|\mathbf{u}\|$ :

$$\mathbf{u} = (\mathcal{R}_k^+)^T [\mathcal{R}_k^+ (\mathcal{R}_k^+)^T]^{-1} [\mathbf{x}(k) - \mathbf{A}^k \mathbf{x}(0)]$$

16. Write the *Heymann Lemma*:

*If  $(\mathbf{A}, \mathbf{B})$  is reachable and if  $\mathbf{b}_i$  is a not zero column of  $\mathbf{B}$ , then it exists a matrix  $\mathbf{M}_i \in \mathcal{R}^{m \times n}$  such that  $(\mathbf{A} + \mathbf{B}\mathbf{M}_i, \mathbf{b}_i)$  is reachable.*

17. Consider a continuous-time nonlinear system  $\dot{\mathbf{x}}(t) = \mathbf{f}(\mathbf{x}(t), \mathbf{u}(t))$  and let  $\mathbf{x}_0$  an equilibrium point of the system for constant input  $\mathbf{u}_0$ . Write the linear part of the Taylor series expansion of the function  $\mathbf{f}(\mathbf{x}(t), \mathbf{u}(t))$  in the neighborhood of point  $(\mathbf{x}_0, \mathbf{u}_0)$ :

$$\mathbf{f}(\mathbf{x}, \mathbf{u}) = \underbrace{\mathbf{f}(\mathbf{x}_0, \mathbf{u}_0)}_0 + \frac{\partial \mathbf{f}(\mathbf{x}, \mathbf{u})}{\partial \mathbf{x}} \Big|_{(\mathbf{x}_0, \mathbf{u}_0)} (\mathbf{x} - \mathbf{x}_0) + \frac{\partial \mathbf{f}(\mathbf{x}, \mathbf{u})}{\partial \mathbf{u}} \Big|_{(\mathbf{x}_0, \mathbf{u}_0)} (\mathbf{u} - \mathbf{u}_0) + \mathbf{h}_1(\mathbf{x}, \mathbf{u})$$

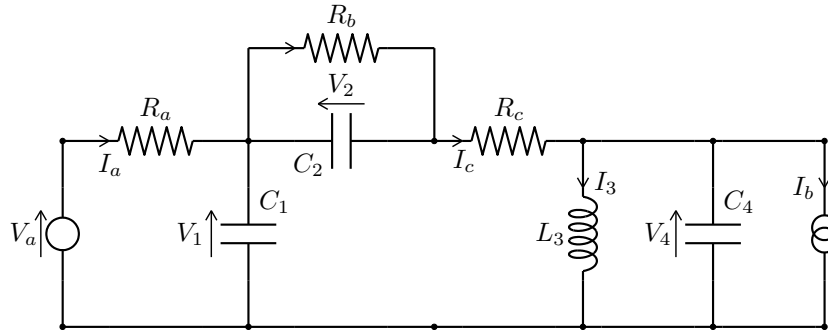
18. Compute the 3 equilibrium points  $\bar{\mathbf{x}}_1$ ,  $\bar{\mathbf{x}}_2$  and  $\bar{\mathbf{x}}_3$  of the following *continuous-time* nonlinear system:

$$\begin{cases} \dot{x}_1(t) = x_2(t) \\ \dot{x}_2(t) = x_1(t)(x_1^2(t) - 1) - 2x_2(t) \end{cases} \quad \xRightarrow{\dot{\mathbf{x}}=0} \quad \begin{cases} \bar{\mathbf{x}}_1 = (0, 0) \\ \bar{\mathbf{x}}_2 = (1, 0) \\ \bar{\mathbf{x}}_3 = (-1, 0) \end{cases}$$

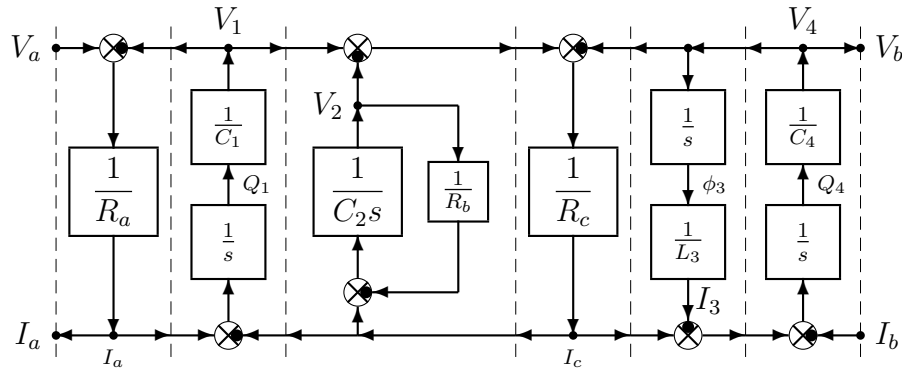
19. Compute the 3 equilibrium points  $\tilde{\mathbf{x}}_1$ ,  $\tilde{\mathbf{x}}_2$  and  $\tilde{\mathbf{x}}_3$  of the following *discrete-time* nonlinear system:

$$\begin{cases} x_1(k+1) = x_2(k) \\ x_2(k+1) = x_1(k)(x_1^2(k) - 1) - 2x_2(k) \end{cases} \quad \xRightarrow{\mathbf{x}(k+1)=\mathbf{x}(k)} \quad \begin{cases} \tilde{\mathbf{x}}_1 = (0, 0) \\ \tilde{\mathbf{x}}_2 = (2, 2) \\ \tilde{\mathbf{x}}_3 = (-2, -2) \end{cases}$$

20. Consider the following electric circuit composed by the capacities  $C_1, C_2, C_4$ , the inductance  $L_3$  and the resistances  $R_a, R_b$  and  $R_c$ . Two inputs act on the system: the voltage  $V_a$  and the current  $I_b$ . The outputs of the system are: the current  $I_a$  and the voltage  $V_b$ .



The POG model of the given electric circuit has the following structure:



Let  $\mathbf{x} = [V_1 \ V_2 \ I_3 \ V_4]^T$  be the state vector,  $\mathbf{u} = [V_a \ I_b]^T$  the input vector and  $\mathbf{y} = [I_a \ V_b]^T$  the output vector. Write the corresponding dynamic system  $\bar{\mathbf{L}}\dot{\mathbf{x}} = \bar{\mathbf{A}}\mathbf{x} + \bar{\mathbf{B}}\mathbf{u}$  and  $\mathbf{y} = \bar{\mathbf{C}}\mathbf{x} + \bar{\mathbf{D}}\mathbf{u}$  in the state space:

$$\underbrace{\begin{bmatrix} C_1 & 0 & 0 & 0 \\ 0 & C_2 & 0 & 0 \\ 0 & 0 & L_3 & 0 \\ 0 & 0 & 0 & C_4 \end{bmatrix}}_{\bar{\mathbf{L}}} \underbrace{\begin{bmatrix} \dot{V}_1 \\ \dot{V}_2 \\ \dot{I}_3 \\ \dot{V}_4 \end{bmatrix}}_{\dot{\mathbf{x}}} = \underbrace{\begin{bmatrix} -\frac{1}{R_a} - \frac{1}{R_c} & \frac{1}{R_c} & 0 & \frac{1}{R_c} \\ \frac{1}{R_c} & -\frac{1}{R_b} - \frac{1}{R_c} & 0 & -\frac{1}{R_c} \\ 0 & 0 & 0 & 1 \\ \frac{1}{R_c} & -\frac{1}{R_c} & -1 & -\frac{1}{R_c} \end{bmatrix}}_{\bar{\mathbf{A}}} \underbrace{\begin{bmatrix} V_1 \\ V_2 \\ I_3 \\ V_4 \end{bmatrix}}_{\mathbf{x}} + \underbrace{\begin{bmatrix} \frac{1}{R_a} & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & -1 \end{bmatrix}}_{\bar{\mathbf{B}}} \underbrace{\begin{bmatrix} V_a \\ I_b \end{bmatrix}}_{\mathbf{u}}$$

$$\underbrace{\begin{bmatrix} I_a \\ V_b \end{bmatrix}}_{\mathbf{y}} = \underbrace{\begin{bmatrix} -\frac{1}{R_a} & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}}_{\bar{\mathbf{C}}} \mathbf{x} + \underbrace{\begin{bmatrix} \frac{1}{R_a} & 0 \\ 0 & 0 \end{bmatrix}}_{\bar{\mathbf{D}}} \underbrace{\begin{bmatrix} V_a \\ I_b \end{bmatrix}}_{\mathbf{u}}$$

21. Write the energy variables  $q_1, q_2$  and the output power variables  $v_1$  and  $v_2$  of the dynamic elements  $\mathcal{D}_1$  and  $\mathcal{D}_1$  that characterize the energetic domains:

	Electrical	Mech. Trans.	Mech. Rot.	Hydraulic
$\mathcal{D}_1$	$C$ Capacity	$M$ Mass	$J$ Inertia	$C_I$ Hydr. Capacity
$q_1$	$Q$ Charge	$p$ Momentum	$p$ Ang. Momentum	$V$ Volume
$v_1$	$V$ Voltage	$v$ Velocity	$\omega$ Ang. Velocity	$P$ Pressure
$\mathcal{D}_2$	$L$ Inductance	$E$ Elasticity	$E$ Tor. Elasticity	$L_I$ Hydr. Inductance
$q_2$	$\phi$ Flux	$x$ Displacement	$\theta$ Ang. Displacement	$\phi_I$ Huder. Flux
$v_2$	$I$ Current	$F$ Force	$\tau$ Torque	$Q$ Volume flow rate

22. Given the following discrete-time nonlinear system  $\mathbf{x}(k+1) = \mathbf{f}(\mathbf{x}(k))$ :

$$\begin{cases} x_1(k+1) &= \alpha x_2(k) - x_1^2(k)x_2(k) \\ x_2(k+1) &= -\alpha x_1(k) + x_1(k)x_2^2(k) \end{cases}$$

It is easy to verify that the origin  $\mathbf{x}_1 = (0, 0)$  is an equilibrium point for the system.

a) Compute the Jacobian  $\mathbf{A}(\mathbf{x}) = \frac{\partial \mathbf{f}(\mathbf{x})}{\partial \mathbf{x}}$  of the nonlinear system:

The Jacobian  $\mathbf{A}(\mathbf{x})$  has the following structure:

$$\mathbf{A}(\mathbf{x}) = \frac{\partial \mathbf{f}(\mathbf{x})}{\partial \mathbf{x}} = \begin{bmatrix} -2x_1x_2 & \alpha - x_1^2 \\ -\alpha + x_2^2 & 2x_1x_2 \end{bmatrix},$$

b) Compute the matrix  $\mathbf{A}_1$  of the linearized system at the point  $\mathbf{x}_1 = (0, 0)$ :

The matrix  $\mathbf{A}_1$  of the linearized system has the following structure:

$$\mathbf{A}_1 = \begin{bmatrix} 0 & \alpha \\ -\alpha & 0 \end{bmatrix}$$

c) Study, for varying parameter  $\alpha$ , the stability of the nonlinear discrete system in the neighborhood of point  $\mathbf{x}_1 = (0, 0)$  using the reduced Lyapunov criterion:

The characteristic polynomial and the eigenvalues of matrix  $\mathbf{A}_1$  are:

$$\Delta_{\mathbf{A}_1}(z) = z^2 + \alpha^2 = 0 \quad \rightarrow \quad z_{1,2} = \pm j\alpha$$

The considered system is a discrete-time system. Using the reduced Lyapunov criterion it can be stated that for  $|\alpha| > 1$  the equilibrium point  $\mathbf{x}_1 = (0, 0)$  of the nonlinear system is unstable, while for  $|\alpha| < 1$  the equilibrium point  $\mathbf{x}_1$  is asymptotically stable. For  $|\alpha| = 1$  the criterion cannot be used.

d) For  $\alpha = 1$ , study the stability of the nonlinear system in the vicinity of the origin  $\mathbf{x}_1 = (0, 0)$  using the “direct” Lyapunov criterion and the function:  $V(\mathbf{x}(k)) = x_1^2(k) + x_2^2(k)$ . Eventually, use the La Salle - Krasowskii criterion.

In the neighbourhood of the origin the function  $V(\mathbf{x}(k)) = x_1^2(k) + x_2^2(k)$  is surely positive definite. Set  $\alpha = 1$ , the function  $\Delta V(\mathbf{x}(k))$  computed along the system's trajectories is the following:

$$\begin{aligned}
\Delta V(\mathbf{x}(k)) &= V(\mathbf{x}(k+1)) - V(\mathbf{x}(k)) \\
&= (x_2 - x_1^2 x_2)^2 + (-x_1 + x_1 x_2^2)^2 - x_1^2 - x_2^2 \\
&= x_2^2 + x_1^4 x_2^2 - 2x_1^2 x_2^2 + x_1^2 + x_1^2 x_2^4 - 2x_1^2 x_2^2 - x_1^2 - x_2^2 \\
&= x_1^4 x_2^2 - 4x_1^2 x_2^2 + x_1^2 x_2^4 = x_1^2 x_2^2 (-4 + x_1^2 + x_2^2) \leq 0
\end{aligned}$$

The function  $\Delta V(\mathbf{x}(k))$  is negative semidefinite and therefore, using the “direct” Lyapunov criterion, it can be stated that in the vicinity of the origin the nonlinear system is stable. The set  $\mathcal{N} = \{(\alpha, 0), \alpha \in R\} \cup \{(0, \beta), \beta \in R\}$  of all the points that nullify the function  $\Delta V(\mathbf{x}(k))$  contains perturbed trajectories of the system. In fact, when  $(x_1, x_2) \in \mathcal{N}$  the given system simplifies as follows:

$$\begin{cases} x_1(k+1) = x_2(k) \\ x_2(k+1) = -x_1(k) \end{cases} \Rightarrow \begin{cases} \mathbf{x}(k+1) = \mathbf{A}\mathbf{x}(k) & \Rightarrow \mathbf{x}(k) = \mathbf{A}^k \mathbf{x}_0, \text{ where} \\ \mathbf{A}^k = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix}^k = \begin{bmatrix} \cos(\frac{k\pi}{2}) & \sin(\frac{k\pi}{2}) \\ -\sin(\frac{k\pi}{2}) & \cos(\frac{k\pi}{2}) \end{bmatrix} \end{cases}$$

For each  $\mathbf{x}_0 \in \mathcal{N}$ , the solution of the system is periodic and therefore it can be stated that for  $\alpha = 1$  the nonlinear system is simply stable in the vicinity of the origin.